

Cheiron School

September 11, 2007 @SPring-8

# X-ray Monochromator

SPring-8/JASRI  
Shunji Goto

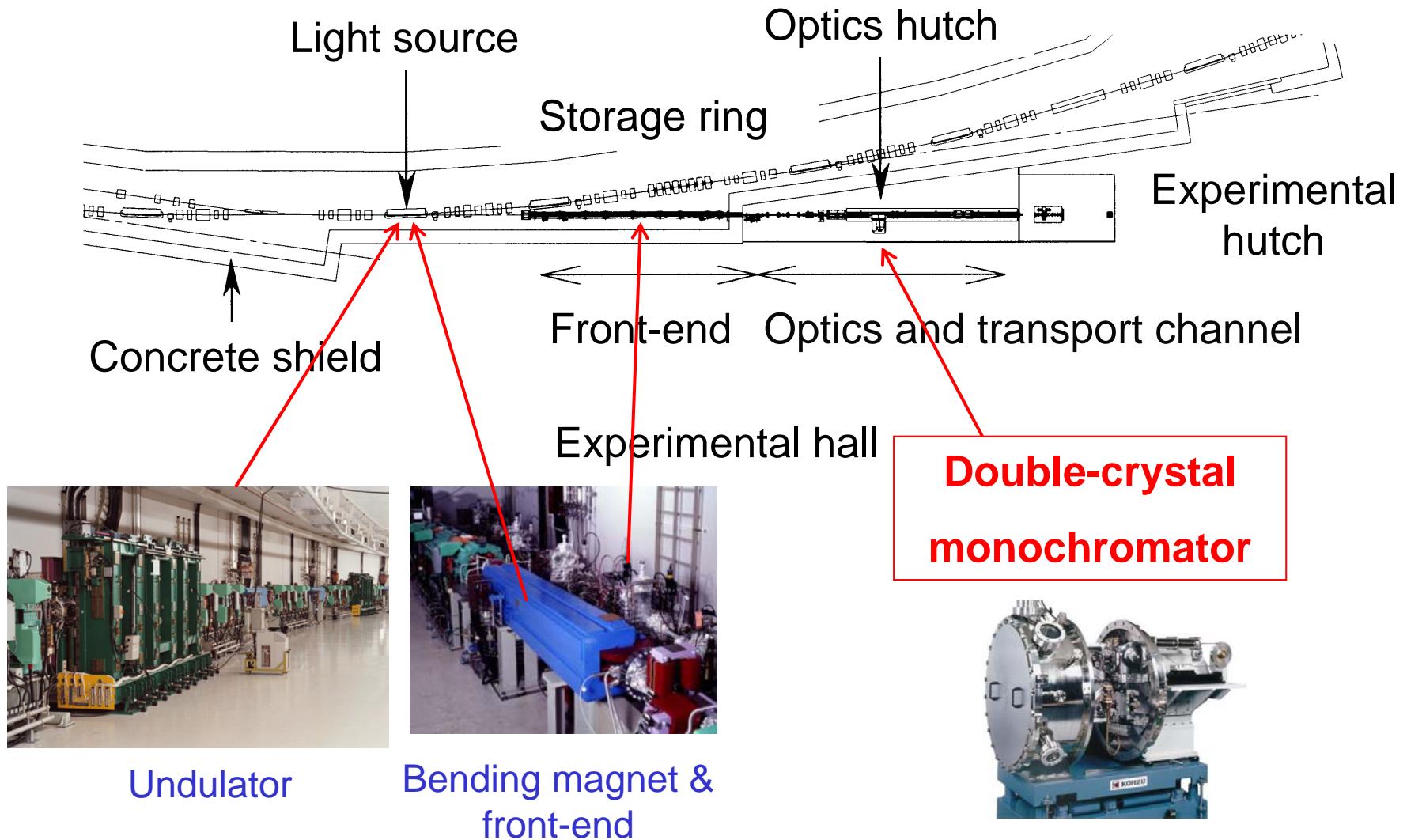
# Outline

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- X-ray beamlines at SPring-8
- Fundamental of x-ray monochromator
  - Bragg's law, Dynamical theory,..
  - Double crystal monochromator
  - Crystal cooling
- Other topics

# **X-ray beamlines at SPring-8**

# Example of beamline structure @SPring-8



# SPring-8 x-ray beamlines with monochromator (1)

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<i>Bemline name</i>		<i>Optics</i>
BL01B1	XAFS	CM (V) + <b>DCM</b> + FM (V)
BL02B1	Single Crystal Structure Analysis	CM (V) + <b>DCM</b> + FM (V)
BL02B2	Powder Diffraction	CM (V) + <b>DCM</b>
BL04B2	High Energy X-ray Diffraction	<b>SBM (H)</b>
BL05SS	Accelerator Beam Diagnosis	<b>DCM</b>
BL08W	High Energy Inelastic Scattering	<b>SBM (V) &amp; SBM (H)</b>
BL08B2	Hyogo BM	CM (V) + <b>DCM</b> + FM (V)
BL09XU	Nuclear Resonant Scattering	<b>DCM + HRM</b>
BL10XU	High Pressure Research	<b>DCM + Double mirror (V)</b>
BL11XU	JAEA Quantum Dynamics	<b>DCM + HRM</b>
BL12XU	NSRRC ID	<b>DCM + CM (V) + HRM + FM (V)</b> <b>&amp; SBM (H)</b>
BL12B2	NSRRC BM	CM (V) + <b>DCM</b> + FM (V)
BL13XU	Surface and Interface Structure	<b>DCM + Tandem FM (H)</b>

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**DCM** : Double-crystal monochromator

**SBM** : Single-bounce monochromator

**HRM** : High-resolution monochromator

**CM** : Collimator mirror

**FM** : Focusing mirror

**V** : Vertical deflection

**H** : Horizontal deflection

# SPring-8 x-ray beamlines with monochromator (2)

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<i>Bemline name</i>	<i>Optics</i>	
BL14B1	CM (V) + <b>DCM</b> + FM (V)	
BL14B2	<b>DCM</b> + FM (V)	
BL15XU	Tandem <b>DCM</b>	
BL16XU	<b>DCM</b> + FM (V)	
BL16B2	<b>DCM</b> + FM (V)	
BL19LXU	<b>DCM</b> + Tandem FM (V)	Medium-length beamline
BL19B2	<b>DCM</b> + Tandem FM (V)	Medium-length beamline
BL20XU	<b>DCM</b>	Medium-length beamline
BL20B2	<b>DCM</b>	1st medium-length beamline
BL22XU	Tandem <b>DCM</b>	
BL24XU	<b>DCM</b> & <b>DCM</b> & <b>DCM</b>	
BL26B1	<b>DCM</b> + FM (V)	
BL26B2	<b>DCM</b> + FM (V)	
BL29XU	<b>DCM</b> + Tandem FM (V)	1st 1-km-long beamline

**DCM** : Double-crystal monochromator

**SBM** : Single-bounce monochromator

**HRM** : High-resolution monochromator

**CM** : Collimator mirror

**FM** : Focusing mirror

**V** : Vertical deflection

**H** : Horizontal deflection

# SPring-8 x-ray beamlines with monochromator (3)

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<i>Bemline name</i>	<i>Optics</i>
BL32B2	<b>DCM + FM (V)</b>
BL35XU	<b>DCM + HRM + FM (V)</b>
BL37XU	<b>DCM + Tandem FM (H) &amp; SBM</b>
BL38B1	<b>DCM + FM (V)</b>
BL38B2	<b>DCM</b>
BL39XU	<b>DCM + FM (H)</b>
BL40B2	<b>DCM + FM (V)</b>
BL41XU	<b>DCM + K-B mirror</b>
BL44XU	<b>DCM + FM (H)</b>
BL44B2	<b>DCM + FM (V)</b>
BL45XU	<b>DCM + K-B mirror</b>
BL46XU	<b>DCM</b>
BL47XU	<b>DCM + Tandem FM (V)</b>

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**DCM** : Double-crystal monochromator

**SBM** : Single-bounce monochromator

**HRM** : High-resolution monochromator

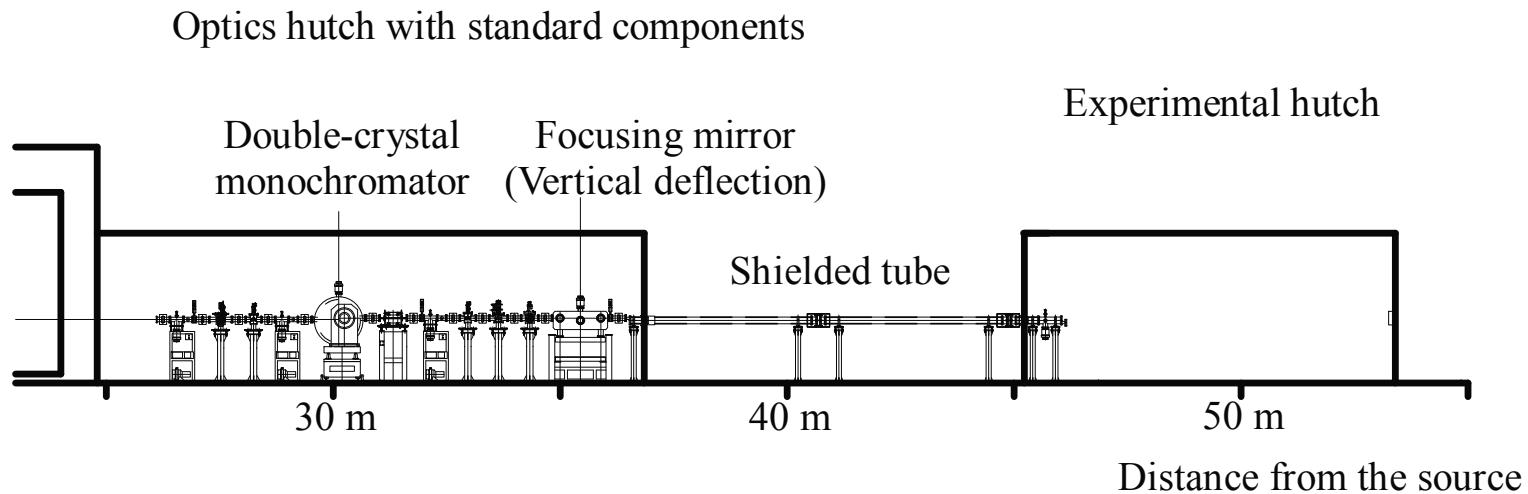
**CM** : Collimator mirror

**FM** : Focusing mirror

**V** : Vertical deflection

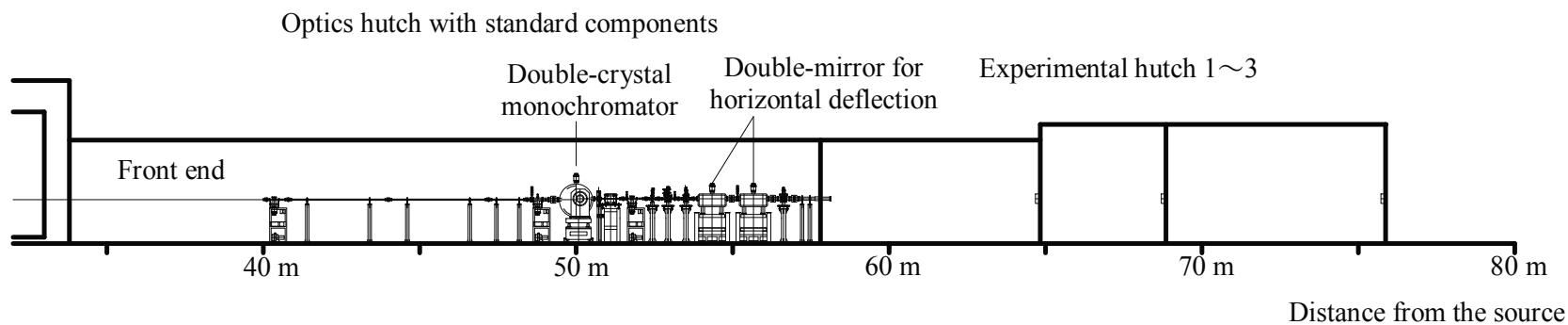
**H** : Horizontal deflection

# Structural biology III, BL38B1



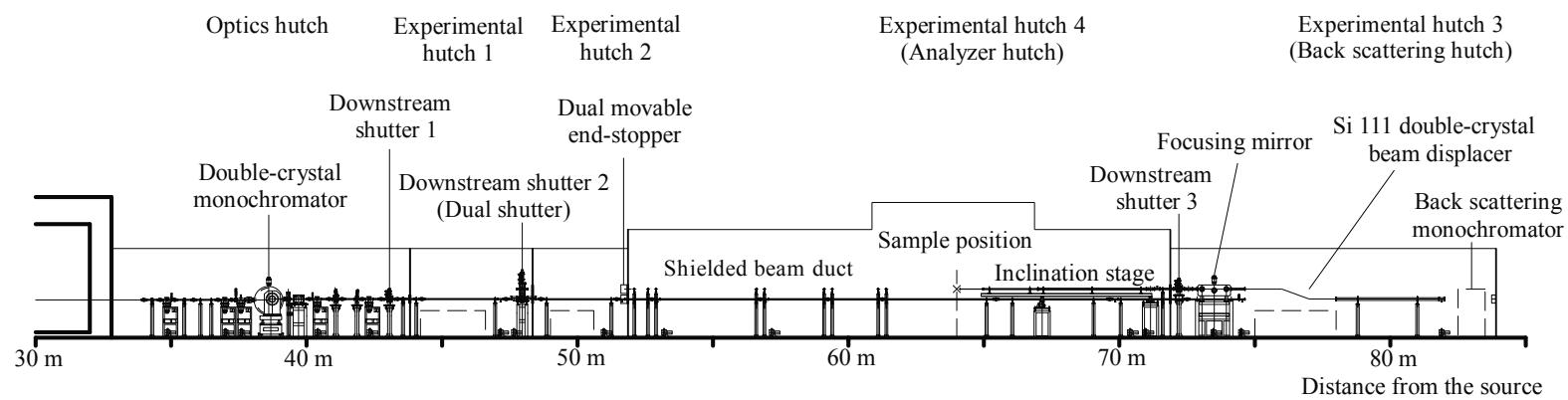
**DCM + FM (V)**

# Surface and interface structure, BL13XU



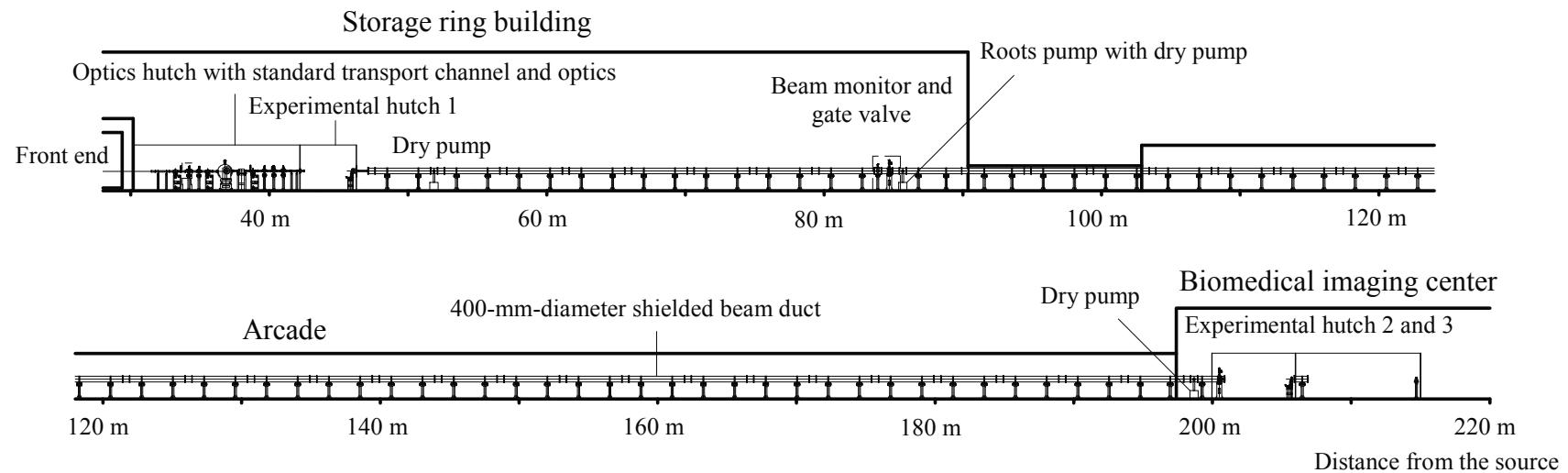
**DCM + tandem FM (H)**

# High resolution inelastic scattering, BL35XU



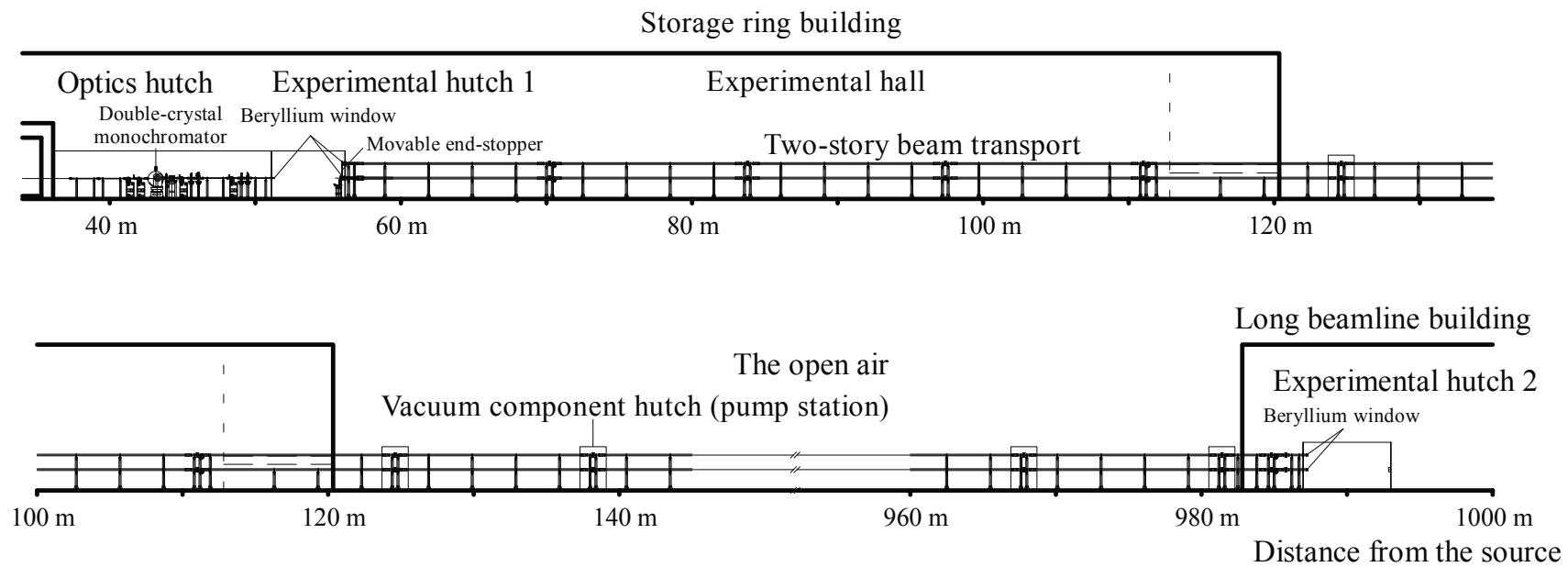
**DCM + HRM + FM (V)**

# Medical imaging I, BL20B2



DCM

# 1 km beamline, BL29XU



**DCM + tandem FM (V)**

# Monochromators @SPring-8

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Beamlines with x-ray monochromator =

**40 / 49 beamlines**

**Double-crystal monochromator:**      43

**Single-bounce monochromator:**      5

**High-resolution monochromator:**      ~4

**X-ray monochromator is key component  
for x-ray beamline.**

# **Fundamental of X-ray monochromator**

# X-ray monochromator using perfect crystal

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## → Principle of monochromator

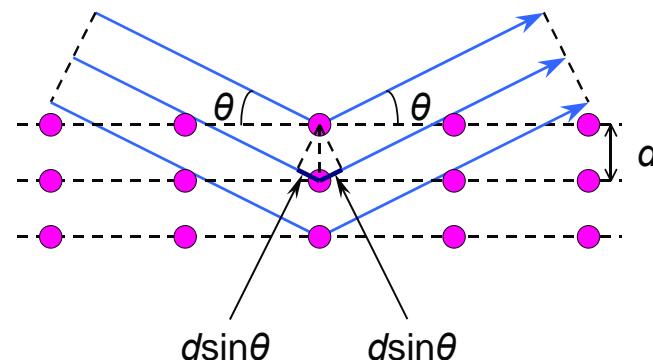
Bragg reflection from perfect single crystal

$$2d \sin \theta = n \lambda$$

$d$ : Lattice ( $d$ )-spacing,

$\theta$ : glancing angle,

$\lambda$ : X-ray wavelength



## → Crystal: silicon, diamond,..

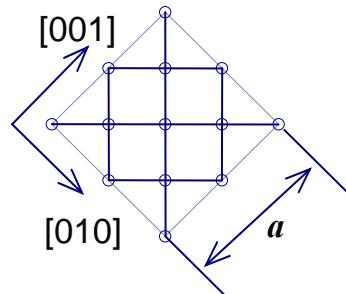
# Requirements for X-ray monochromator

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- Monochromatize x-rays of required photon energy
  - with required energy width
  - with required throughput (efficiency)
- Fixed-exit beam using double-crystal monochromator
- Focusing using bending mechanism
- Cooling under heat-load from SR beam
- ...

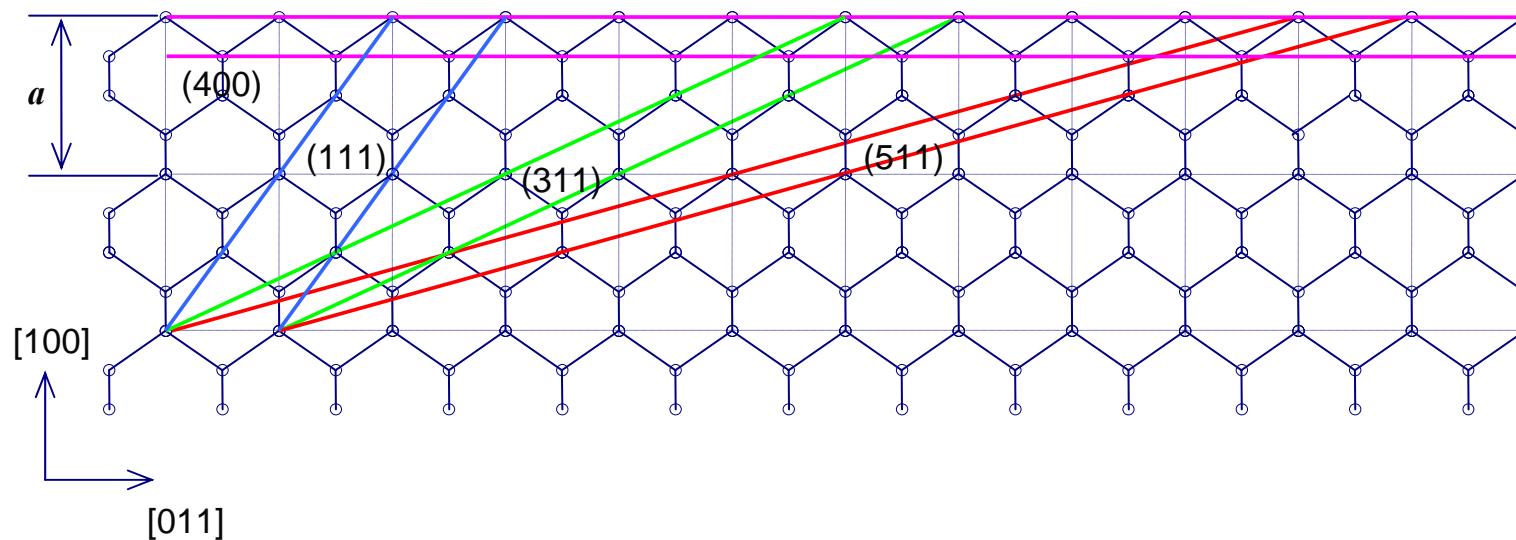
# Lattice planes of silicon

**Top view**



$d$ -spacing
(400) : 1.3578 Å
(111) : 3.1356 Å
(311) : 1.6375 Å
(511) : 1.0452 Å

**Side view**



# Energy range of SPring-8 standard monochromator

e.g. For SPring-8 standard monochromator

→ Reflection

Si 111 refl.

Si 311 refl.

Si 511 refl.

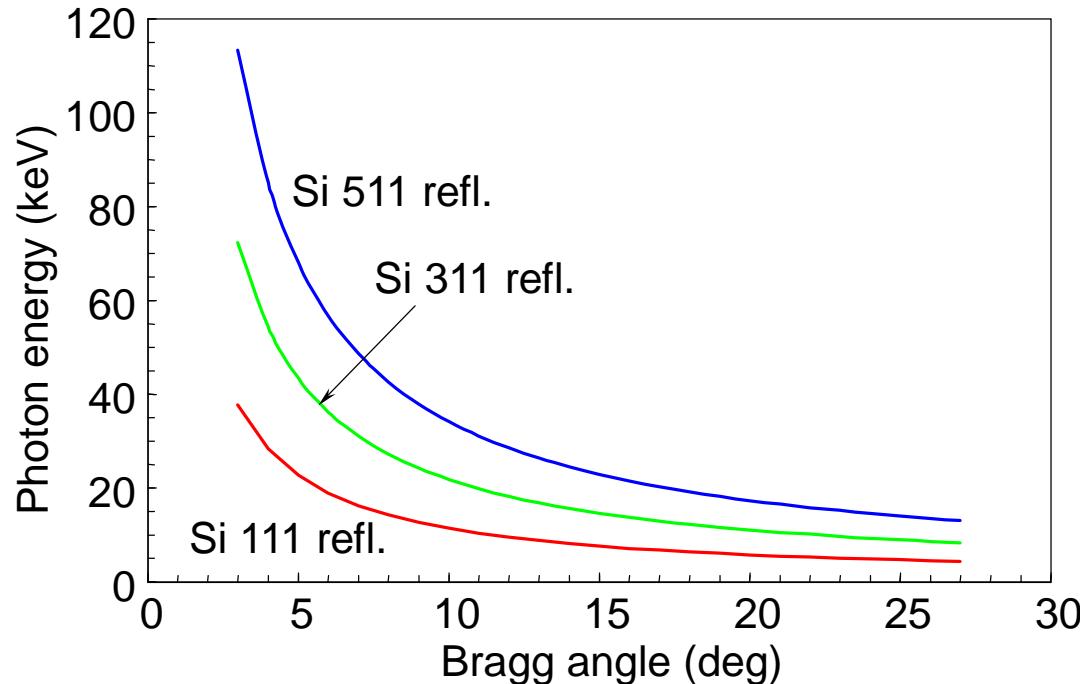
.....

→ Bragg angles

3~27°

→ Energy range

4.4~110 keV



Photon energy (wavelength) can be selected  
by crystal, net planes, and Bragg angle.

# **Dynamical theory**

## **- Two wave case -**

# Two wave equations

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Following two equations are derived using Maxwell's equations for 3-dimensional periodic medium (= perfect single crystal).

$$\begin{aligned}(\mathbf{k}_0^2 - k^2)E_0 - \chi_{-h} P K_0^2 E_h &= 0 \\ (\mathbf{k}_h^2 - k^2)E_h - \chi_h P K_0^2 E_0 &= 0\end{aligned}$$

$$k_h = k_0 + \mathbf{h} : \textbf{\textit{Momentum conservation}}$$

$\mathbf{h}$  : Reciprocal lattice vector

$E_0, E_h$  : Fourier components of electric field

$K_0$  : Incident wave vector in vacuum

$k_0, k_h$  : Refracted and reflected wave vectors in crystal

$k$  : Mean wave number in crystal

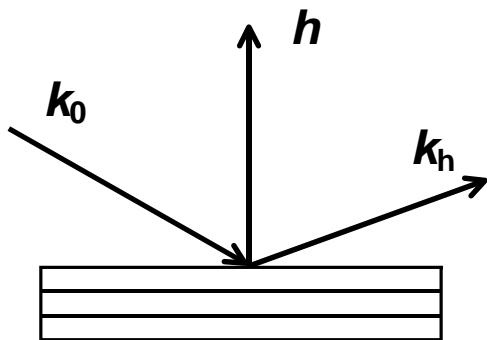
$\chi_0, \chi_h, \dots$  : Fourier components of the polarizability (Negative values,  
 $10^{-6} \sim 10^{-5}$ )

$P$  : Polarization factor ( $\sigma : P = 1, \pi : P = \cos 2\theta_B$ )

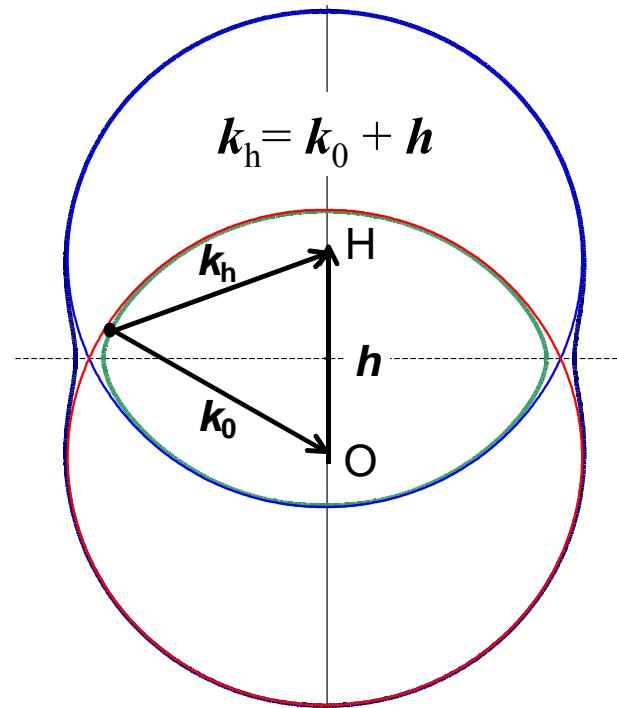
# Dispersion surface

Using two equations, we obtain following :

$$(\mathbf{k}_0^2 - k^2)(\mathbf{k}_h^2 - k^2) = \chi_h \chi_{-h} P^2 K_0^4$$



Real space



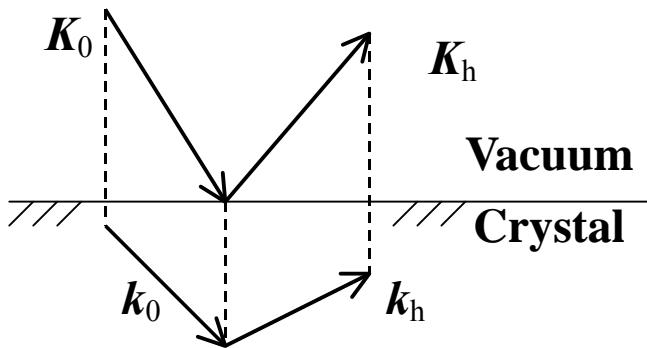
Reciprocal space

Two dispersion surfaces close to two Laue spheres ( $O, H$ ) for each polarization, showing the gap near Bragg condition.

# Boundary condition of wave vector

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First, we must consider connections of waves from vacuum into crystal and from crystal to vacuum, to solve the equations.



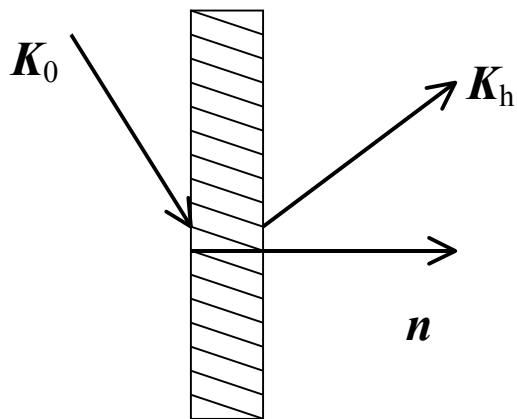
**Tangential component of wave vector must be continuous.**

Incident wave in vacuum

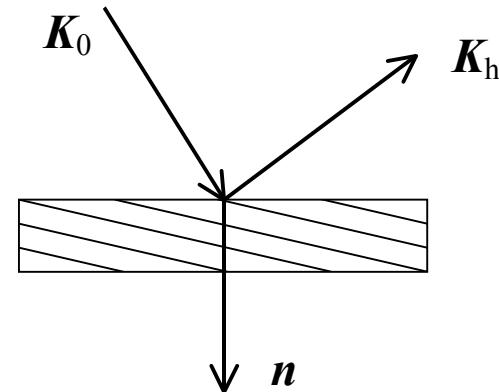
- Refracted wave in crystal
- Bragg reflection
- Reflected wave in the crystal
- Reflected wave in vacuum

# Laue case and Bragg case

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Laue case

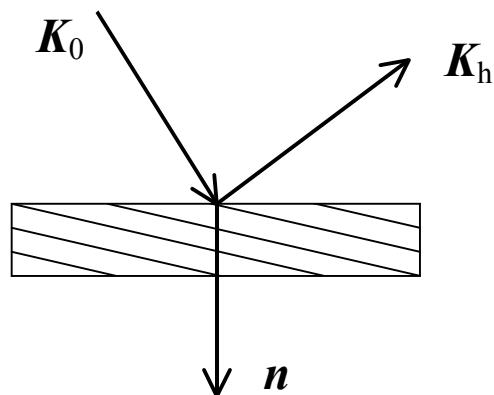


Bragg case

# Asymmetry ratio

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$$\left\{ \begin{array}{l} \gamma_0 = \hat{K}_0 \cdot n \\ \gamma_h = \hat{K}_h \cdot n \end{array} \right. \quad b = \frac{\gamma_0}{\gamma_h}$$



**Laue case:  $b>0$**

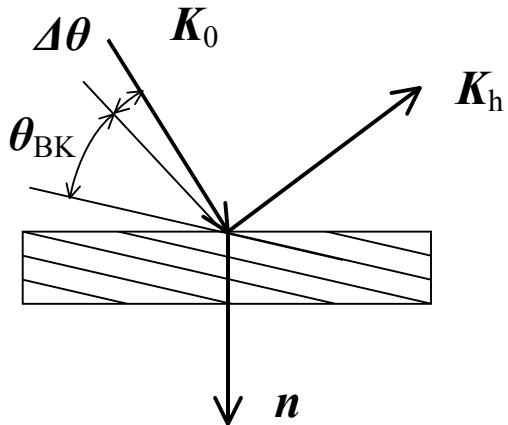
Symmetric Bragg case:  $b=1$

**Bragg case:  $b<0$**

Symmetric Bragg case:  $b=-1$

# Normalized parameter $W$ for deviation from Bragg condition

Parameter  $W$  is related to the gap between two dispersion surfaces and total reflection occurs at  $-1 < W < 1$  for Bragg case.



$\theta_{BK}$  : Kinematical Bragg angle

$\Delta \theta$  : Deviation angle from  $\theta_{BK}$

$K_0, K_h, h$  are in the same plane.

$$W = \left\{ \Delta \theta \sin 2\theta_{BK} + \frac{\chi_{0r}}{2} \left( 1 - \frac{\gamma_h}{\gamma_0} \right) \right\} \sqrt{\frac{\gamma_0}{|\gamma_h|}} \frac{1}{|\chi_{hr}| \cdot |P|}$$

For symmetric Bragg case, sigma polarization:

$$W = \left\{ \Delta \theta \sin 2\theta_{BK} + \chi_{0r} \right\} \frac{1}{|\chi_{hr}|}$$

# Amplitude ratio

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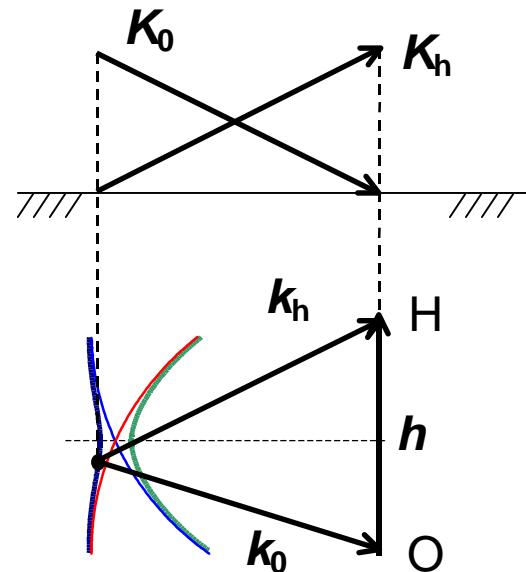
From these equations, we obtain the ratio  $r = E_h/E_0$  as a function of parameter  $W$ .

For Bragg case, no absorption, and thick crystal:

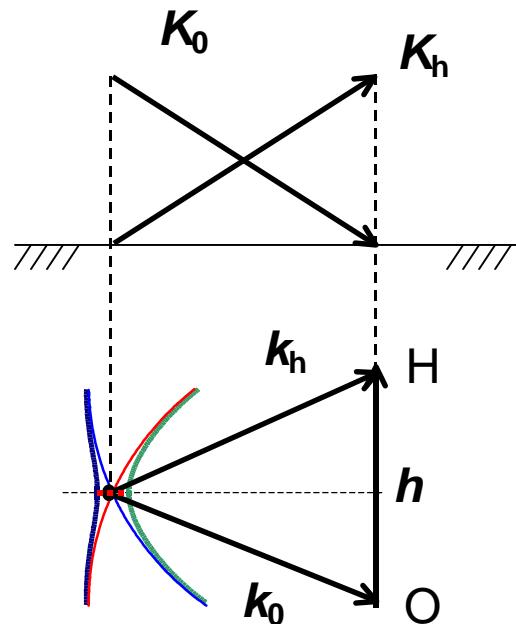
$$\left\{ \begin{array}{l} r = \frac{E_h}{E_0} = -\sqrt{\frac{\gamma_0}{|\gamma_h|}} \frac{|\chi_{hr}|}{\chi_{-h}} \frac{|P|}{P} \left( W + \sqrt{W^2 - 1} \right) \quad (W < -1) \\ \\ r = \frac{E_h}{E_0} = -\sqrt{\frac{\gamma_0}{|\gamma_h|}} \frac{|\chi_{hr}|}{\chi_{-h}} \frac{|P|}{P} \left( W + i\sqrt{1 - W^2} \right) \quad (-1 \leq W \leq 1) \quad \leftarrow \textbf{Total reflection} \\ \\ r = \frac{E_h}{E_0} = -\sqrt{\frac{\gamma_0}{|\gamma_h|}} \frac{|\chi_{hr}|}{\chi_{-h}} \frac{|P|}{P} \left( W - \sqrt{W^2 - 1} \right) \quad (W > 1) \end{array} \right.$$

# Movement of tie point

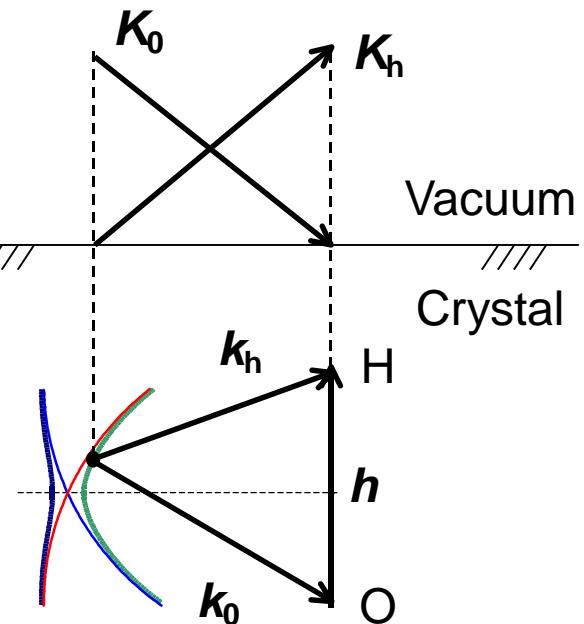
(1) Lower angle  
 $W < -1$



(2) Near Bragg condition  
 $-1 < W < 1$



(3) Higher angle  
 $W > 1$

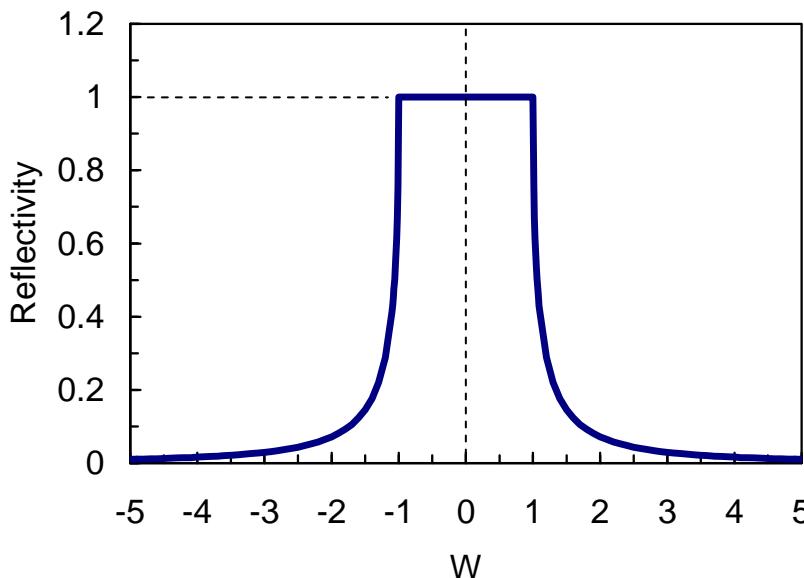


Total reflection

# Reflectivity

Finally, we obtain reflectivity  
for Bragg case, no absorption, and thick crystal:

$$\left\{ \begin{array}{l} R = \frac{|\gamma_h|}{\gamma_0} \left| \frac{E_h}{E_0} \right|^2 = (W + \sqrt{W^2 - 1})^2 \quad (W < -1) \\ R = 1 \quad (-1 \leq W \leq 1) \quad \leftarrow \text{Total reflection} \\ R = (W - \sqrt{W^2 - 1})^2 \quad (W > 1) \end{array} \right.$$



For symmetric Bragg case, sigma polarization:

$$W = \{\Delta\theta \sin 2\theta_{BK} + \chi_{0r}\} \frac{1}{|\chi_{hr}|}$$

Darwin width  $\rightarrow \Delta W = 2$

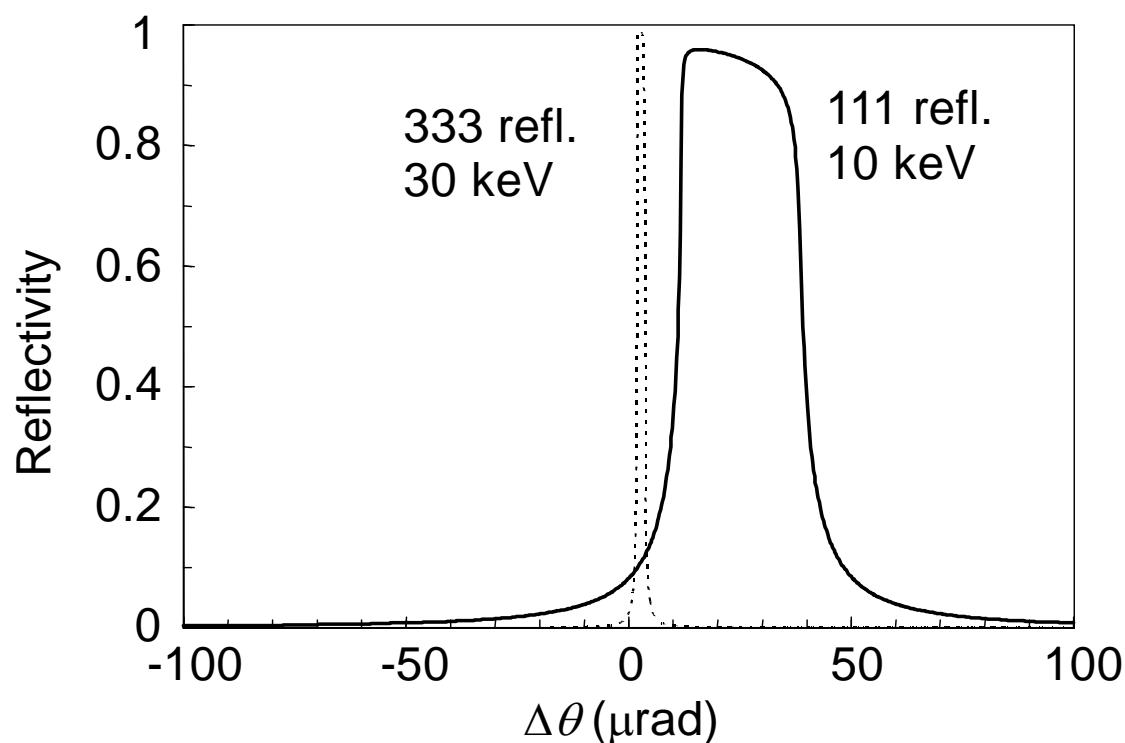
$$\omega = \frac{2|\chi_{hr}|}{\sin 2\theta_{BK}} \propto |F_h|$$

Shift of Bragg angle due to refraction:

$$\Delta\theta_{refraction} = -\frac{\chi_{0r}}{\sin 2\theta_{BK}}$$

# Intrinsic rocking curve for silicon

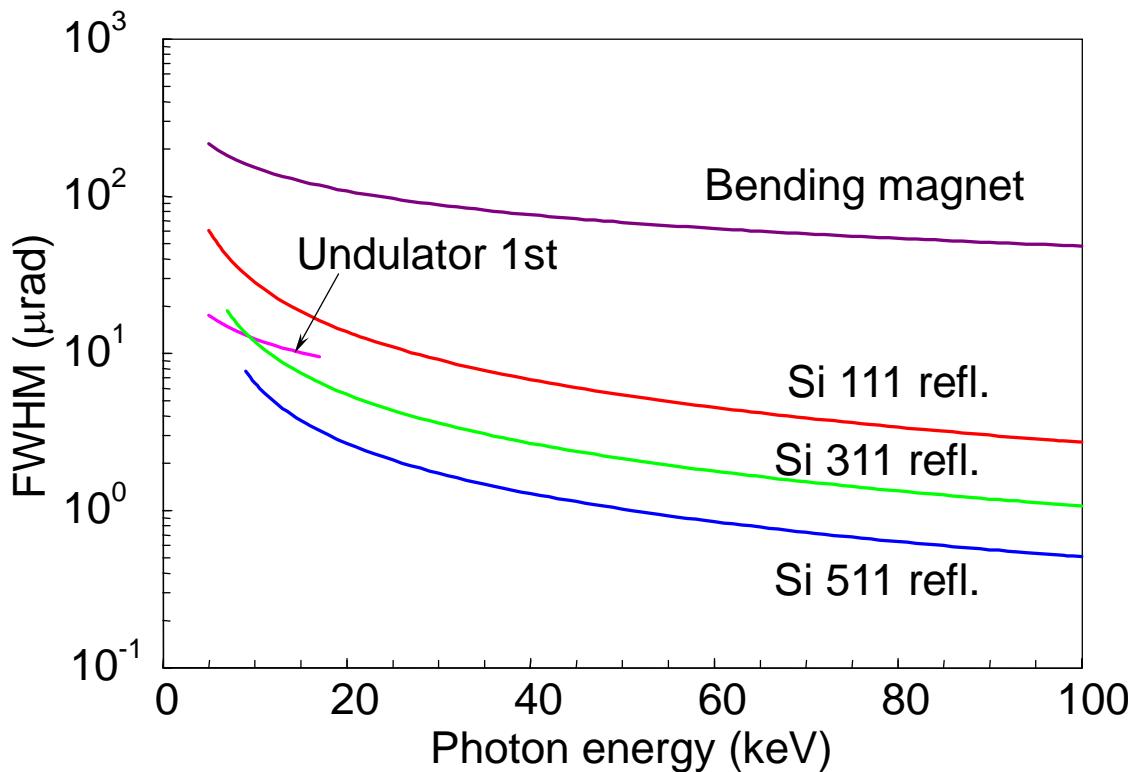
Based on the dynamical theory for perfect crystal  
for thick crystal and absorption considered:



## Features:

- Diffraction width (Darwin width) of  $0.1 \sim 100 \mu\text{rad}$
- Peak reflectivity of  $\sim 1$  for low absorption case

# Angular divergence of sources and diffraction width



SPring-8 bending magnet

$$\sigma_r \approx \frac{1}{\gamma} \approx 60 \mu\text{rad}$$

Undulator ( $N=140$ )

$$\sigma_r \approx \frac{1}{\gamma \sqrt{N}} \approx 5 \mu\text{rad}$$

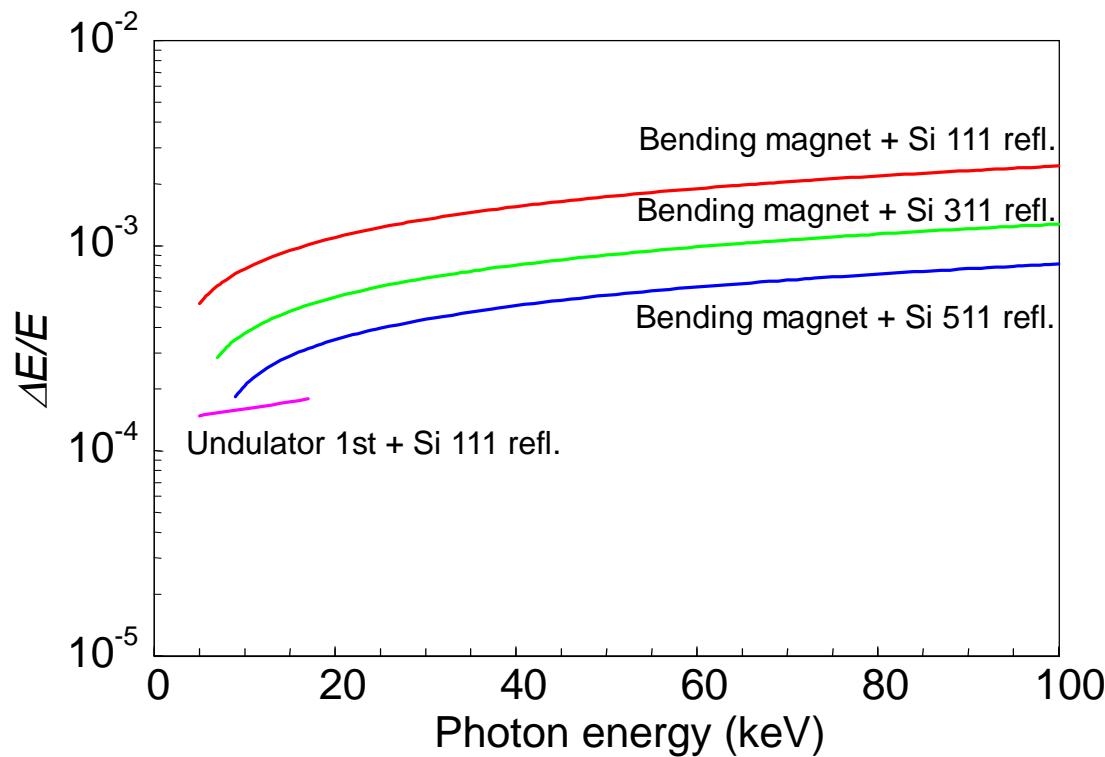
Divergence of undulator radiation is the same order as diffraction width of low order reflection.

# Energy resolution

$$\frac{\Delta E}{E} = \cot \theta_B \sqrt{\Omega^2 + \omega^2}$$

$\Omega$ : divergence of source

$\omega$ : diffraction width



Using slit, collimator mirror,.. we can reduce  $\Omega_{\text{eff}}$ ,

$$\Delta E/E = 10^{-5} \sim 10^{-3}$$

# **Double-crystal monochromator**

# Double crystal monochromator (DCM)

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**Fixed-exit operation of double-crystal monochromator  
is very crucial for end-users of beamlines.**

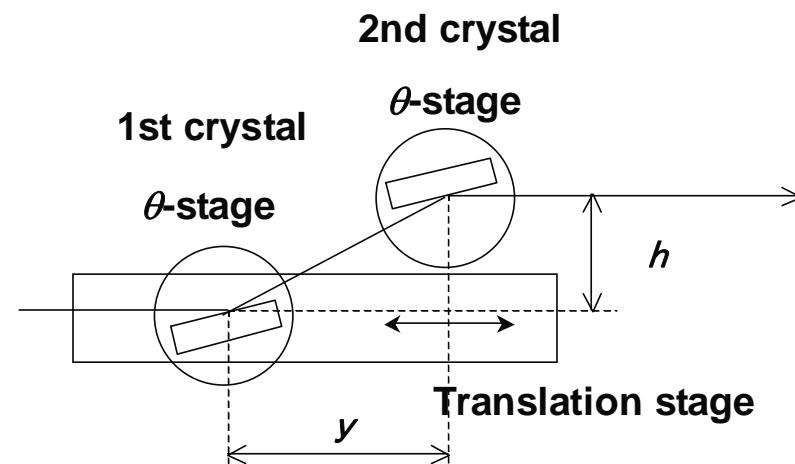
To obtain fixed-exit beam  
independent of Bragg angle:

- Use the same crystals and  $d$ -spacing  
for 1<sup>st</sup> and 2<sup>nd</sup> crystals
- Keep parallel setting

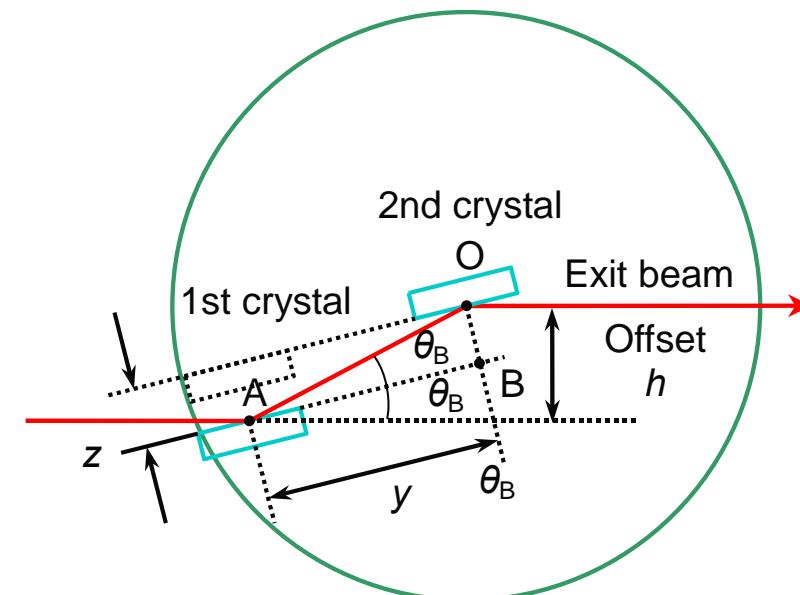
# Fixed-exit by DCM

## Two arrangements for DCM

(1)  $\theta_1$ +translation+ $\theta_2$  link



(2)  $\theta$ +two translation link

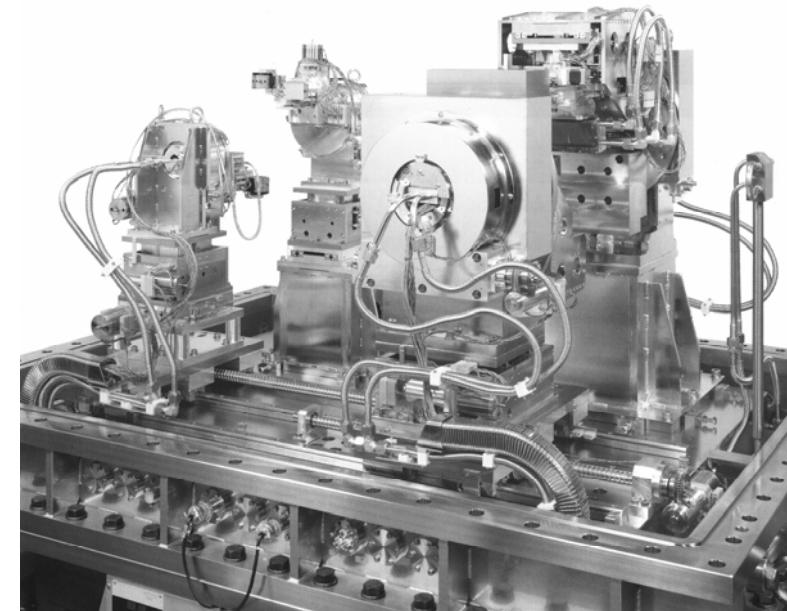
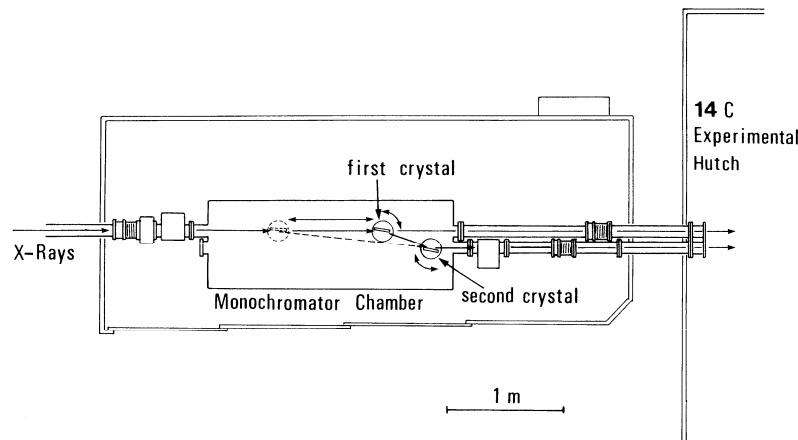


$$y = \frac{h}{\tan 2\theta_B}$$

$$y = AB = \frac{h}{2 \sin \theta_B} \quad z = OB = \frac{h}{2 \cos \theta_B}$$

$$(y^2 - h^2 / 4)(z^2 - h^2 / 4) = h^4 / 16$$

# $\theta_1$ + translation + $\theta_2$ computer link



PF BL-14C

Kawata and Ando, NIM A246 (1986)

$h= 150 \text{ mm}$ ,  $\theta_B = 2.6 \sim 25^\circ$

SPring-8 BL15XU

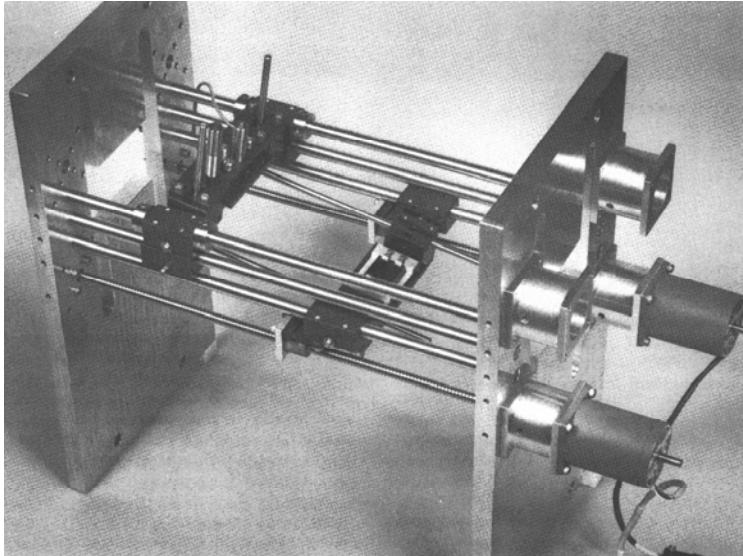
SPring-8 information Vol. 5, No.1 (2000)

$h= 100 \text{ mm}$ ,  $\theta_B = 5.7 \sim 72^\circ$

**Large offset, long-stroke translation**

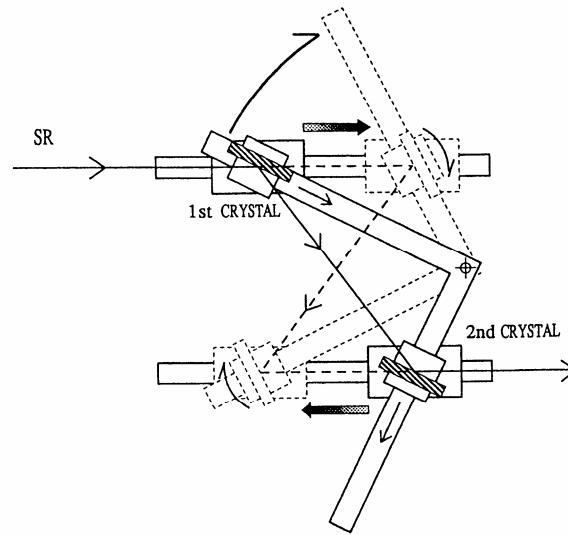
**Difficulty of parallelism between 1st and 2nd crystal**

# Boomerang link type



Kirkland, NIM-A291 (1990)

$h = 50 \text{ mm}$ ,  $\theta_B = 5 \sim 85^\circ$



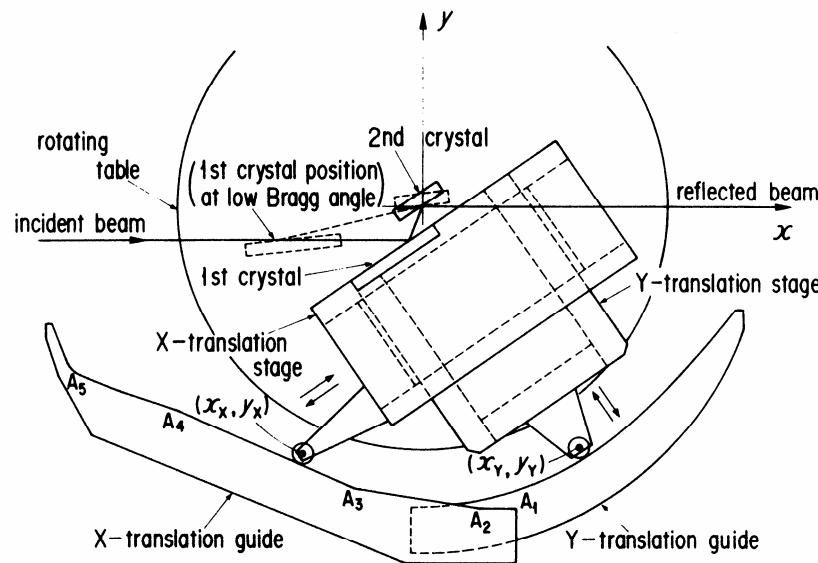
UVSOR BL 1A, BL 7A

Hiraya et al., RSI 66 (1995)

$\theta_B = 18.5 \sim 71.5^\circ$

- Difficulties for crystal cooling and multi-stage adjustment
- Low rigidity

# $\theta +$ two translation (KEK-PF)



PF BL-4C..

Matsushita et al., NIM A246 (1986)

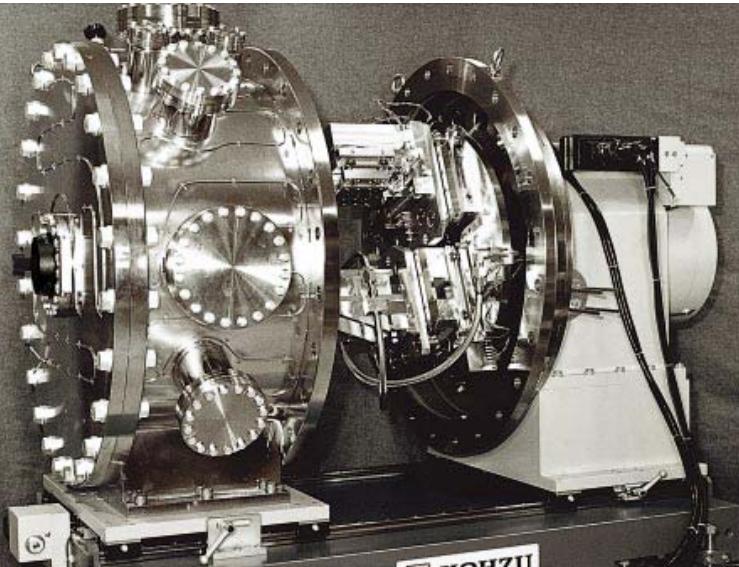
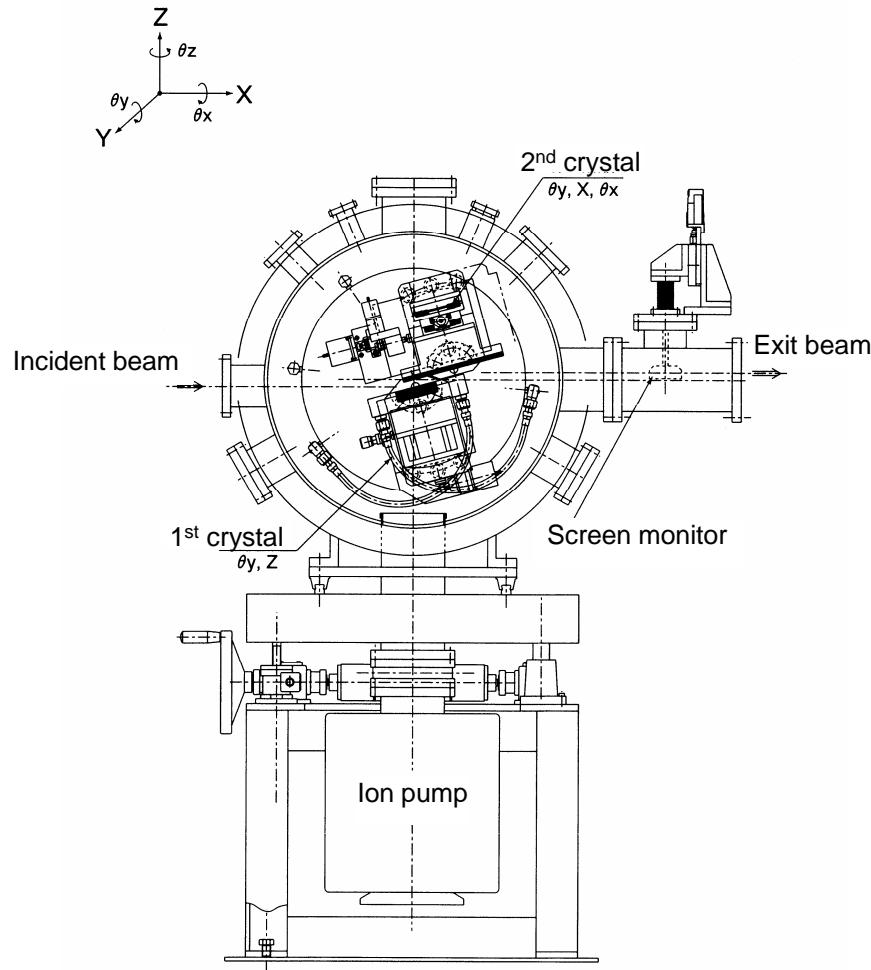


$$h = 25 \text{ mm}, \theta_B = 5 \sim 70^\circ$$

Two cams for two translation-stages

Rotation center at 2<sup>nd</sup> crystal

# $\theta$ + two translation (APS)



$$h = 35 \text{ mm}, \quad \theta_B = 5 \sim 30^\circ$$

$\theta$ -y-z computer link

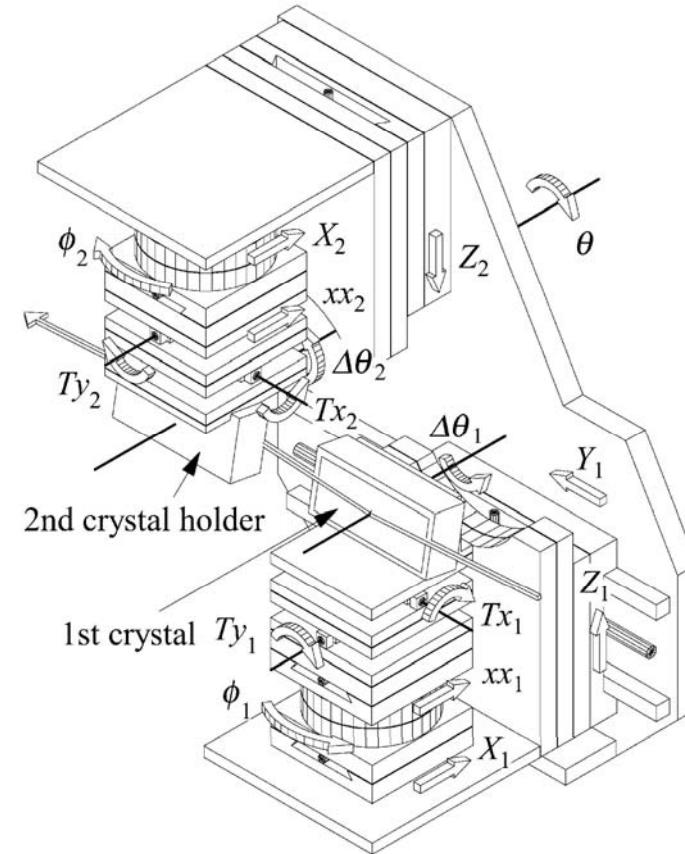
Rotation center at  $h/2$ -height

# SPring-8 standard DCM



$3^\circ < \theta_B < 27^\circ$

Offset  $h = 30$  mm



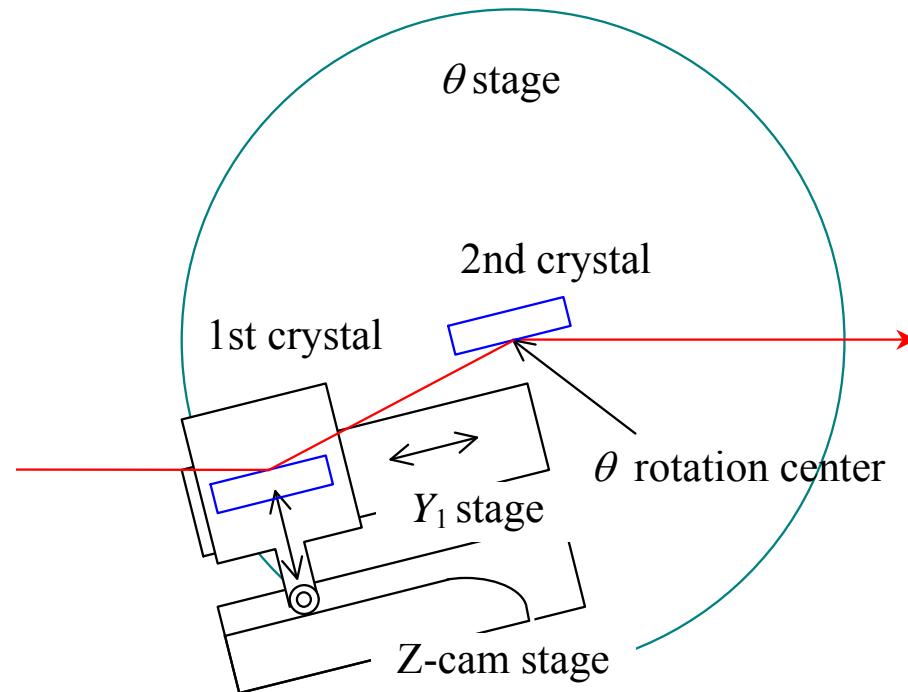
Adjustment stages  
for undulator beamline DCM  
Sub-micron, sub- $\mu$ rad control

# $\theta$ -y-z computer-cam link

$\theta$ -y: linked by computer control  
 $y$ -z: linked by cam

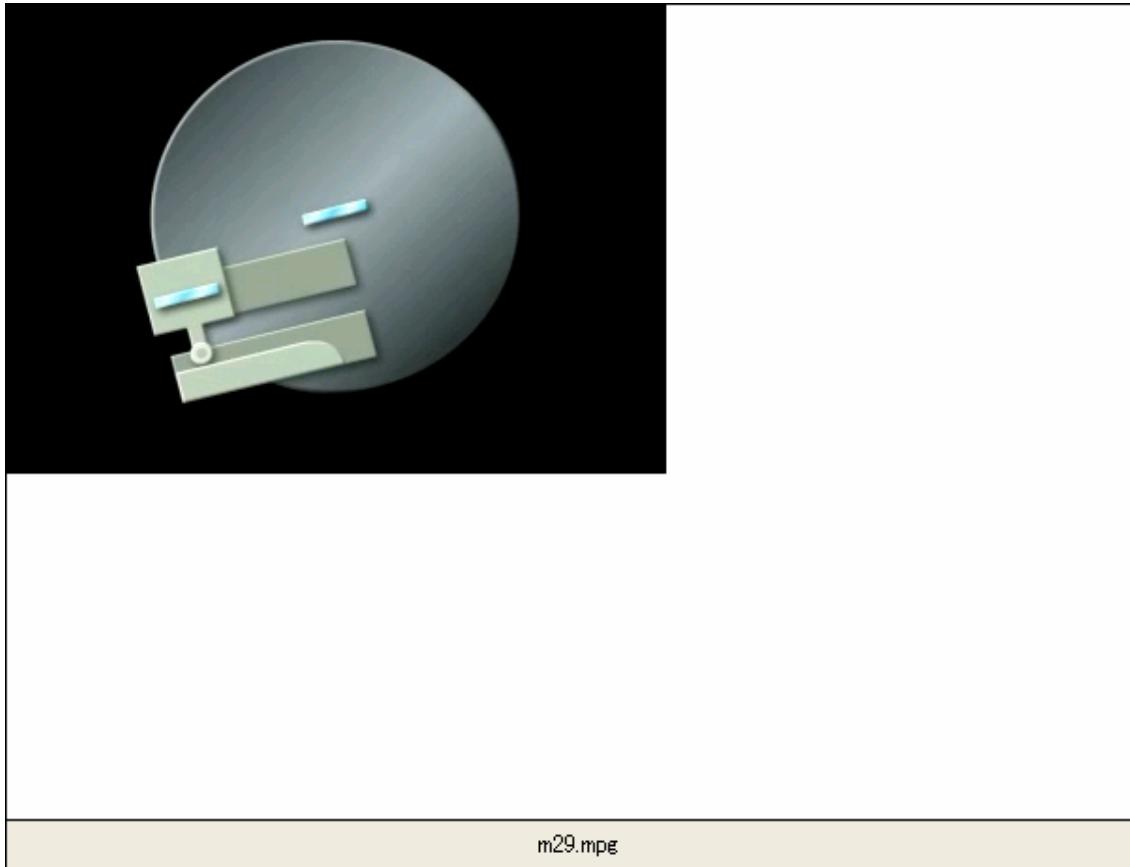
Cam shape for fixed-exit

$$\left( y^2 - \frac{h^2}{4} \right) \left( z^2 - \frac{h^2}{4} \right) = \frac{h^4}{16}$$



# $\theta$ -y computer + y-z cam link

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# **Crystal cooling**

# Heat load on 1<sup>st</sup> Crystal

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**Heat load on the mochromator 1<sup>st</sup> crystal:**

- For SPring-8 bending magnet source  
**100 W & 1 W/mm<sup>2</sup>**
- For SPring-8 standard undulator source  
**~500 W & ~ 500 W/mm<sup>2</sup>**

cf.      Hot plate      : ~ 0.02 W/mm<sup>2</sup>  
              CPU          : ~ 0.3 W/mm<sup>2</sup>

# Crystal cooling

Why crystal cooling ?

$$Q_{in} \text{ (Heat load by SR)} = Q_{out} \text{ (Cooling + Radiation,...)}$$

→ with temperature rise  $\Delta T$

→  $\alpha \Delta T = \Delta d$  ( $d$ -spacing change)

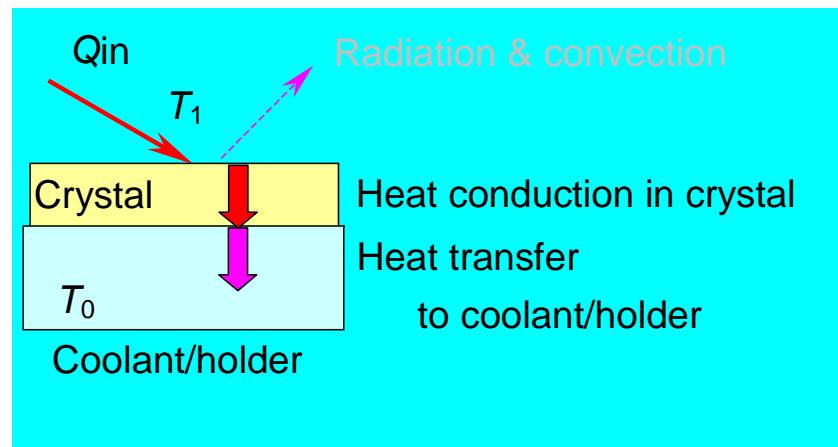
$\alpha$ : thermal expansion coefficient

or →  $\Delta \theta$  (bump of lattice due to heat load)

***Miss-matching between 1st and 2nd crystals occurs:***

→ Thermal drift, Loss of intensity, Broadening of beam, loss of brightness

→ Melting or limit of thermal strain → **Broken !**



# Solution for crystal cooling

---

We must consider:

Thermal expansion of crystal:  $\alpha$ ,

Thermal conductivity in crystal:  $\kappa$ ,

Heat transfer to coolant and crystal holder.

Solutions:

(S-1)  $\kappa/\alpha \rightarrow$  Larger

(S-2) Large contact area between crystal and coolant/holder  
 $\rightarrow$  larger

(S-3) Irradiation area  $\rightarrow$  Larger, and power density  $\rightarrow$  smaller

# Figure of merit

---

	Silicon 300 K	Silicon 80 K	Diamond 300 K
$\kappa$ (W/m/K)	150	1000	2000
$\alpha$ (1/K)	$2.5 \times 10^{-6}$	$-5 \times 10^{-7}$	$1 \times 10^{-6}$
$\kappa / \alpha \times 10^6$	60	2000	2000

Figure of merit of cooling:  
Good for silicon (80 k) and diamond (300 K)

# For SPring-8 case

# Bending magnet beamline

Power and density :  $\sim 100$  W,  $\sim 1$  W/mm<sup>2</sup> @40 m

## Method:

→ Direct cooling with fin crystal

← S-2

# Undulator beamline

(Linear undulator,  $N= 140$ ,  $\lambda_u= 32$  mm)

Power and density :  $\sim 500$  W ,  $\sim 500$  W/mm<sup>2</sup> @40 m

## Methods:

→ Direct cooling of silicon pin-post crystal

← S-2

+ Rotated inclined geometry ( $\rightarrow$  10 W/mm<sup>2</sup>)

← S-3

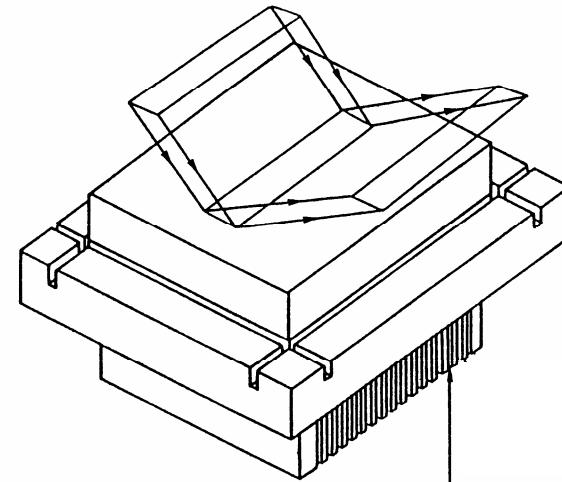
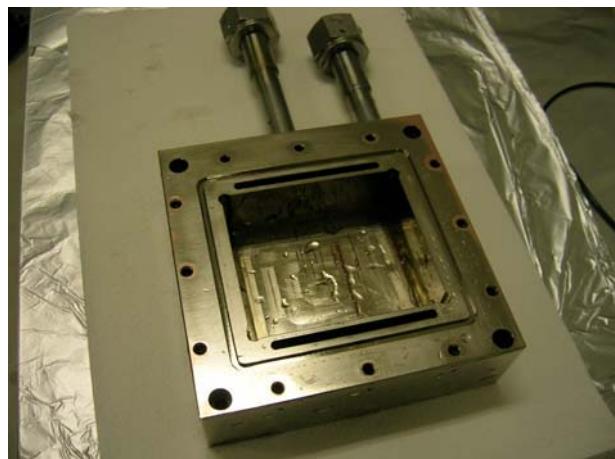
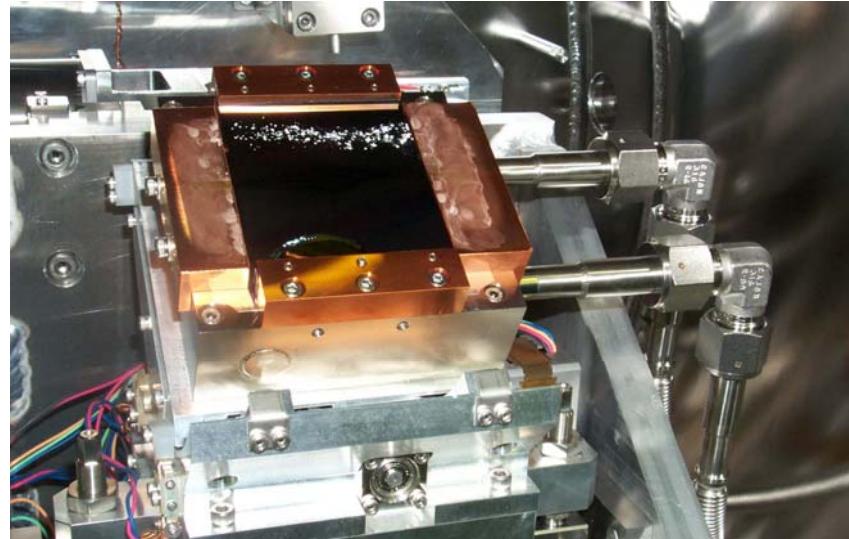
→ or Cryogenic cooling using LN<sub>2</sub> circulation

← S-1

→ or Indirect cooling of IIa diamond crystal

← S-1

# Direct cooling with fin crystal



Fins with  
Inserted metal

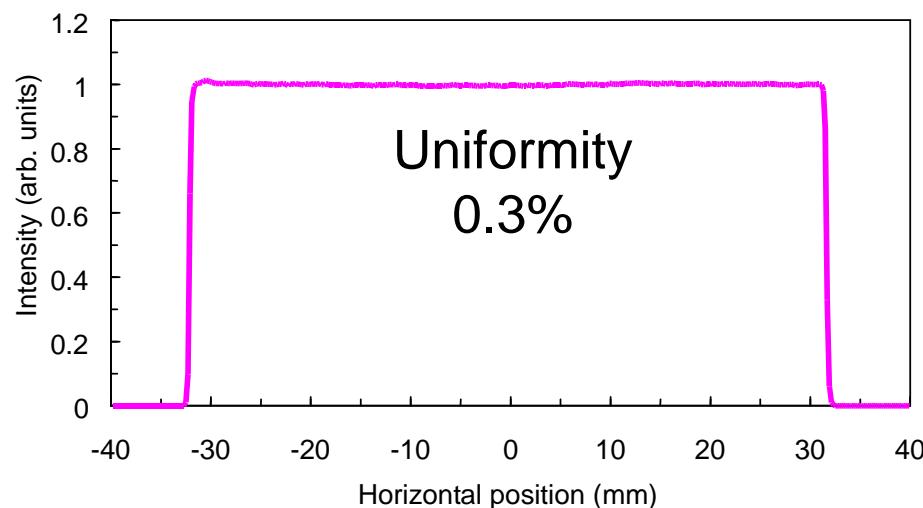
Applied to bending magnet beamline

# Performance of fin crystal (1)



Si 111 refl.

Si 333 refl.



$h\nu = 25 \text{ keV}$

Si 111 refl.

Ring current= 1 mA

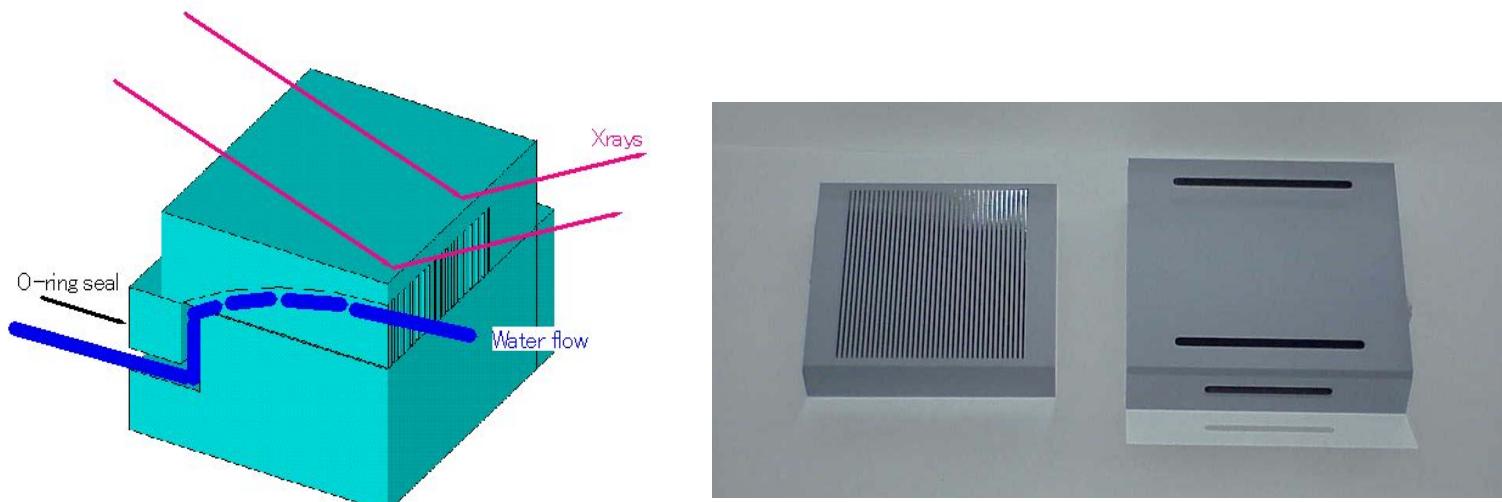
Mechanical deformation removed

# Direct cooling with fin crystal

---

Improvement of fin-cooling crystal

Reduce radiation damage of rubber O-ring

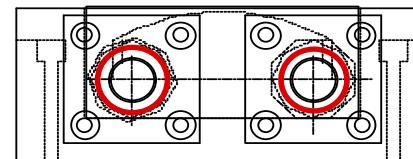
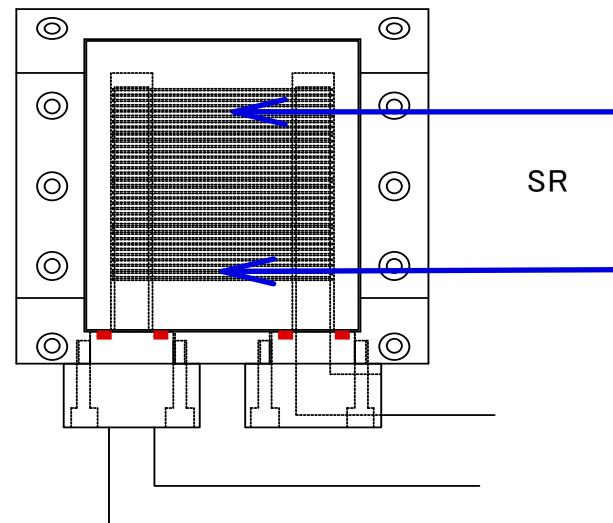
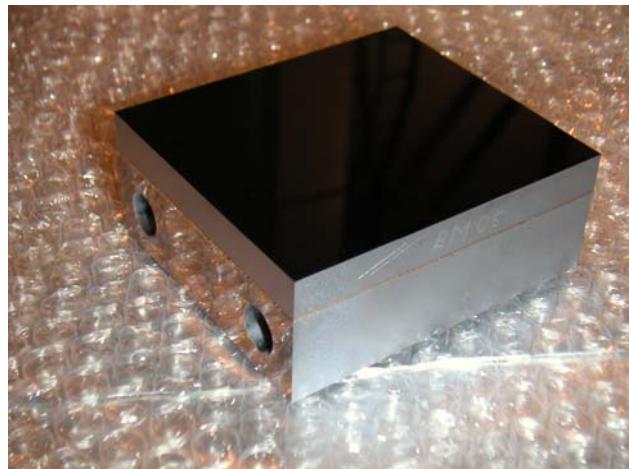


Au-Si eutectic  
bonding

# Direct cooling with fin crystal

---

Reduce radiation damage of rubber O-ring



# Performance of fin crystal (2)

---

X-ray image for Si 311 refl.



$\theta_B = 5^\circ$  ,  $E = 43.4$  keV



$\theta_B = 10^\circ$  ,  $E = 21.8$  keV



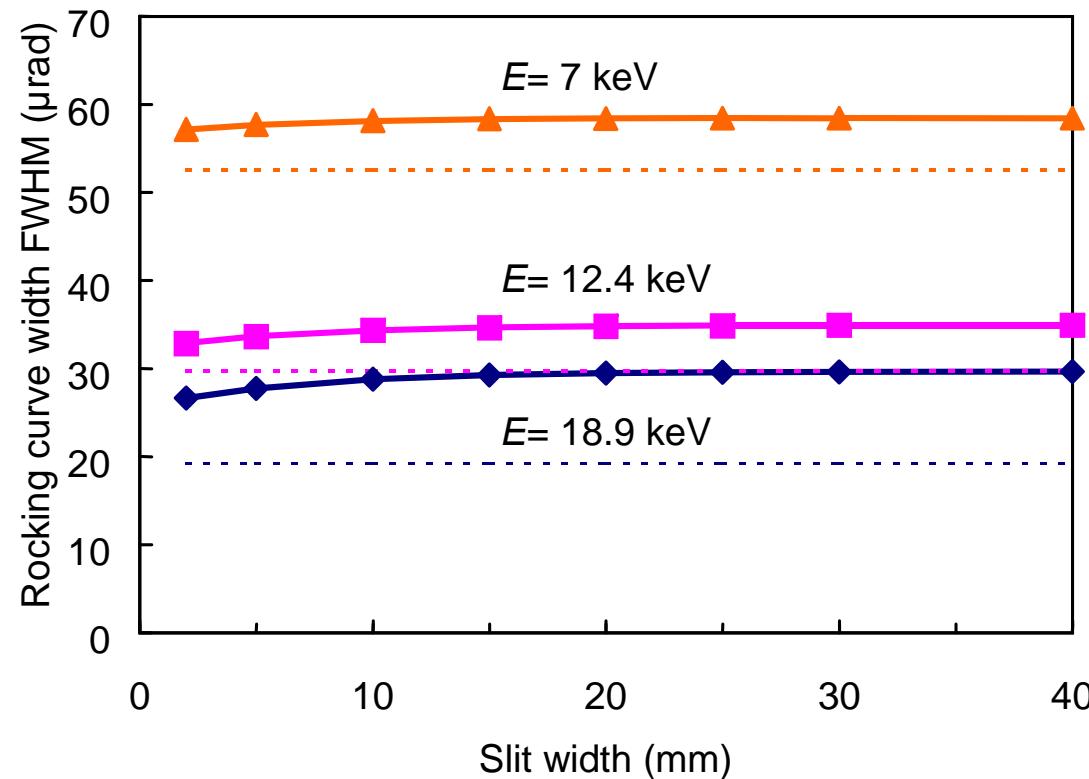
$\theta_B = 20^\circ$  ,  $E = 11.1$  keV

Slit: 3 mm<sup>V</sup> × 40 mm<sup>H</sup>

## Current status

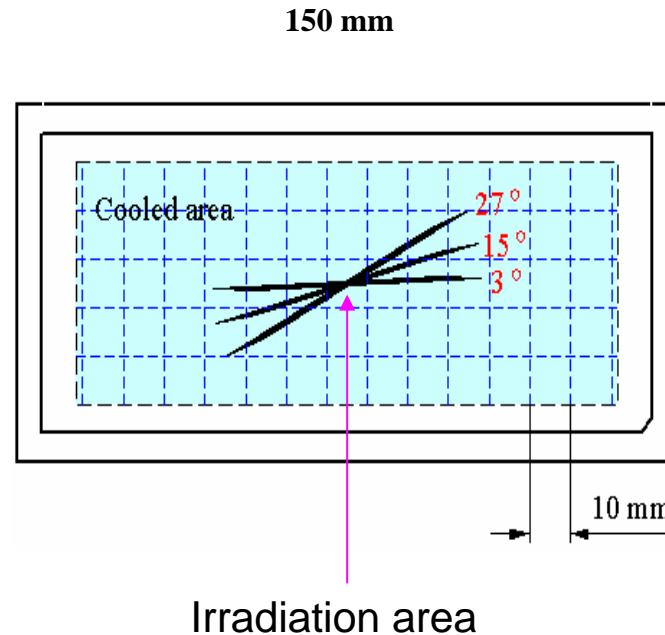
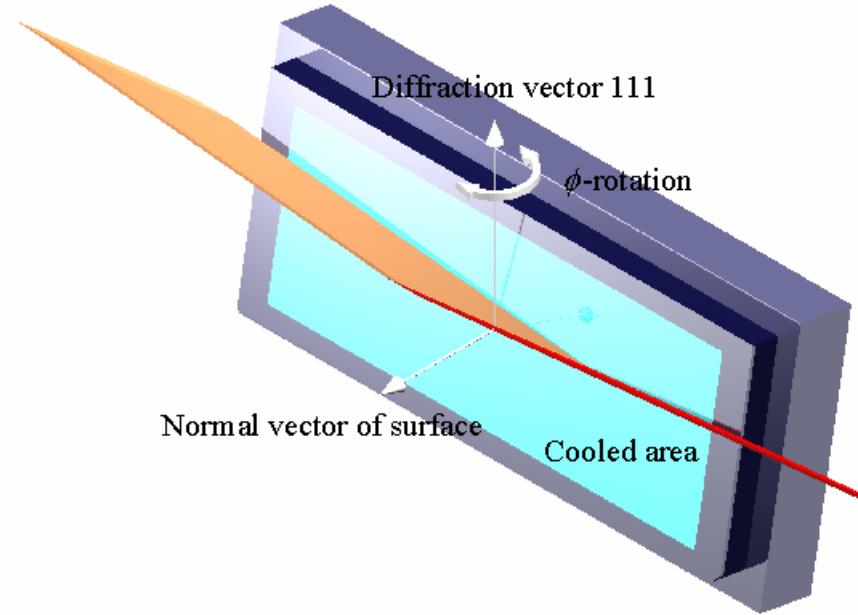
- Practical use both (311) and (111) crystals
- 2~4 sec. twist due to fabrication process must be reduced.
- No heat strain for (111) crystal at 12 keV photon
- Radiation damage of O-ring is improved by side-inlet.
- Durability test is under way.

# Performance of fin crystal (3)



Si 111 refl.  
Ring current= 100 mA

# Direct cooling of silicon pin-post crystal + Rotated inclined geometry



Inclination angle  $\beta = 80^\circ$

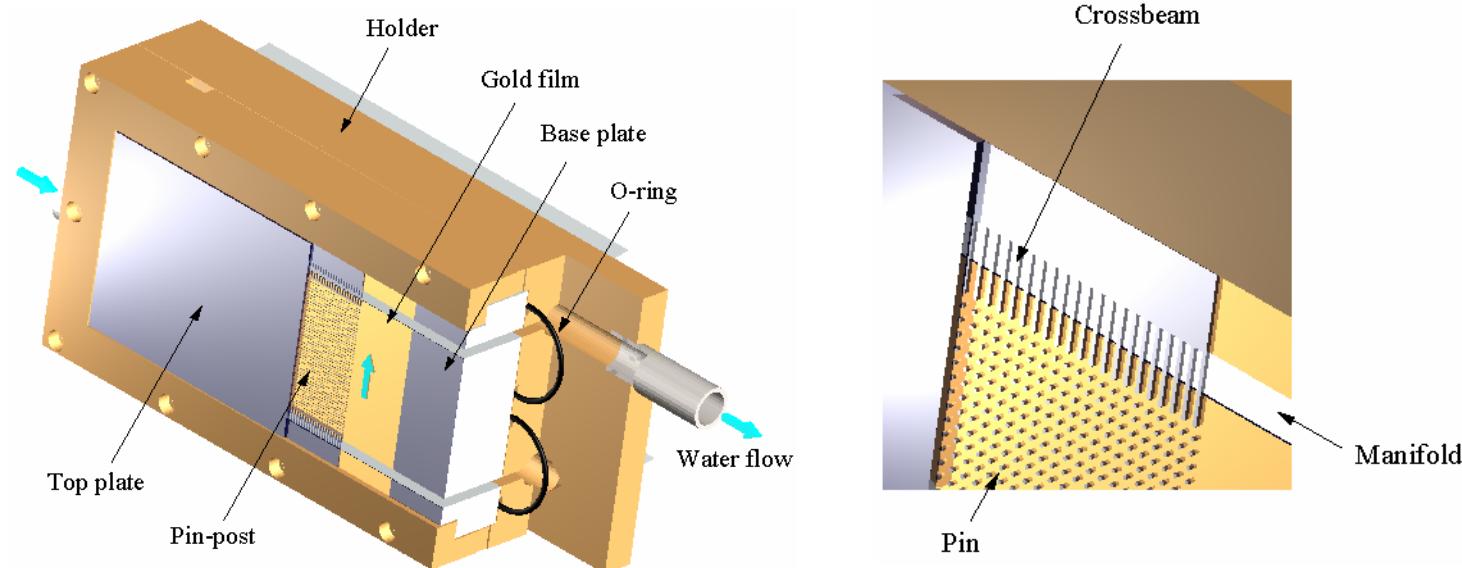
Grazing angle down to  $1^\circ$  using  $\phi$ -rotation

Irradiation area enlarged to x50, power density reduced to 1/50

Applied to undulator beamline

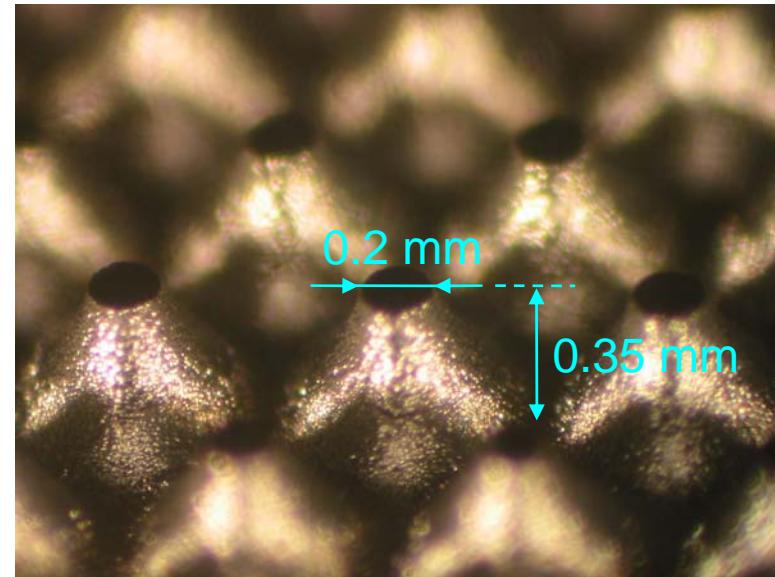
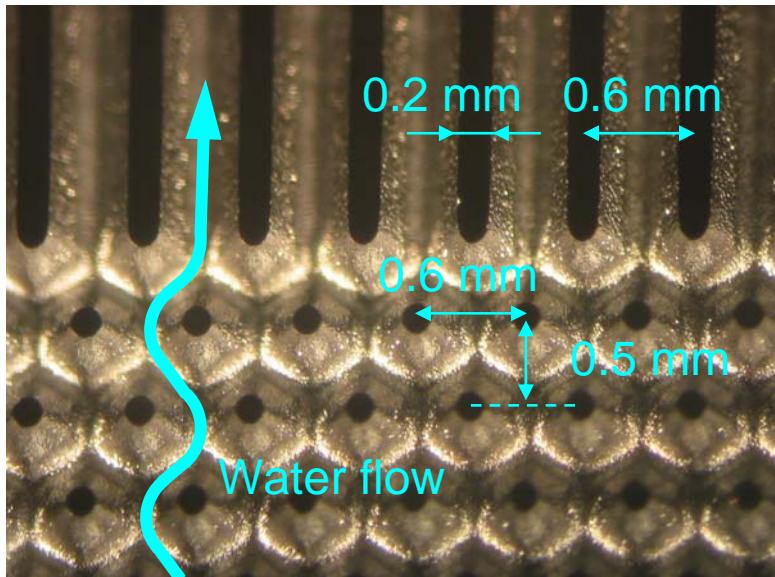
# Structure of pin-post crystal

Top plate with pin-post is bonded to base plate (manifold) using Au-Si eutectic bonding.



# Pin-post structure

---

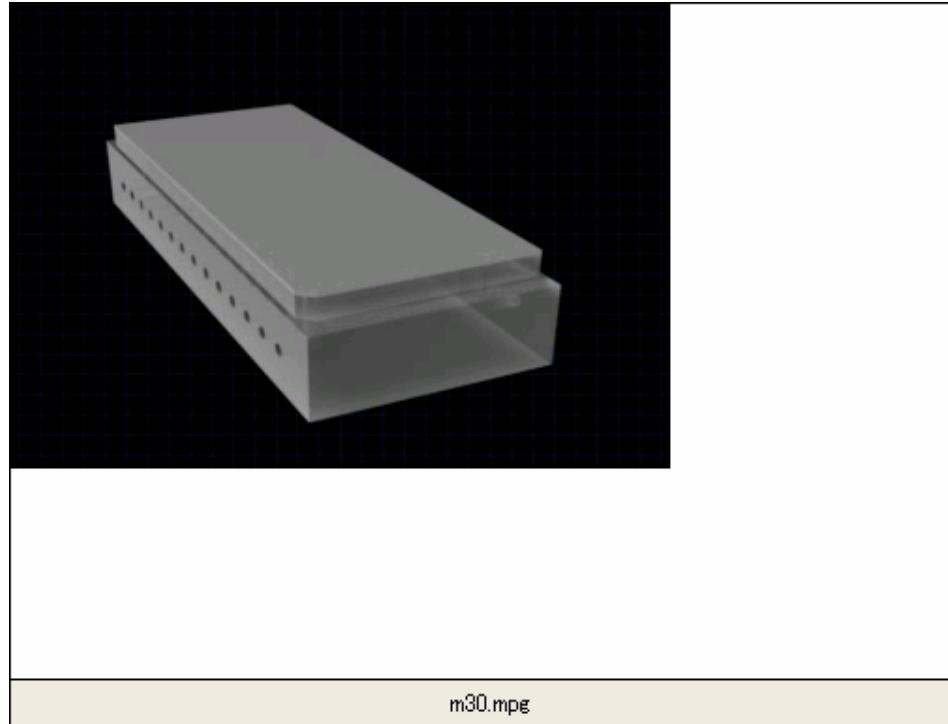


Fine pins are fabricated to increase cooling efficiency.

Limitation of sandblast

# Water flow in the pin-post crystal

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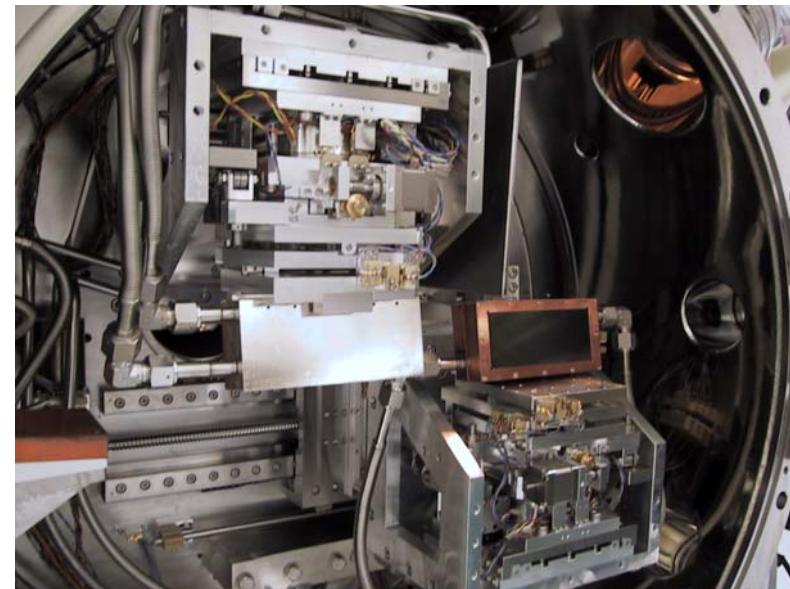
m30.mpg

# DCM with pin-post crystal

---



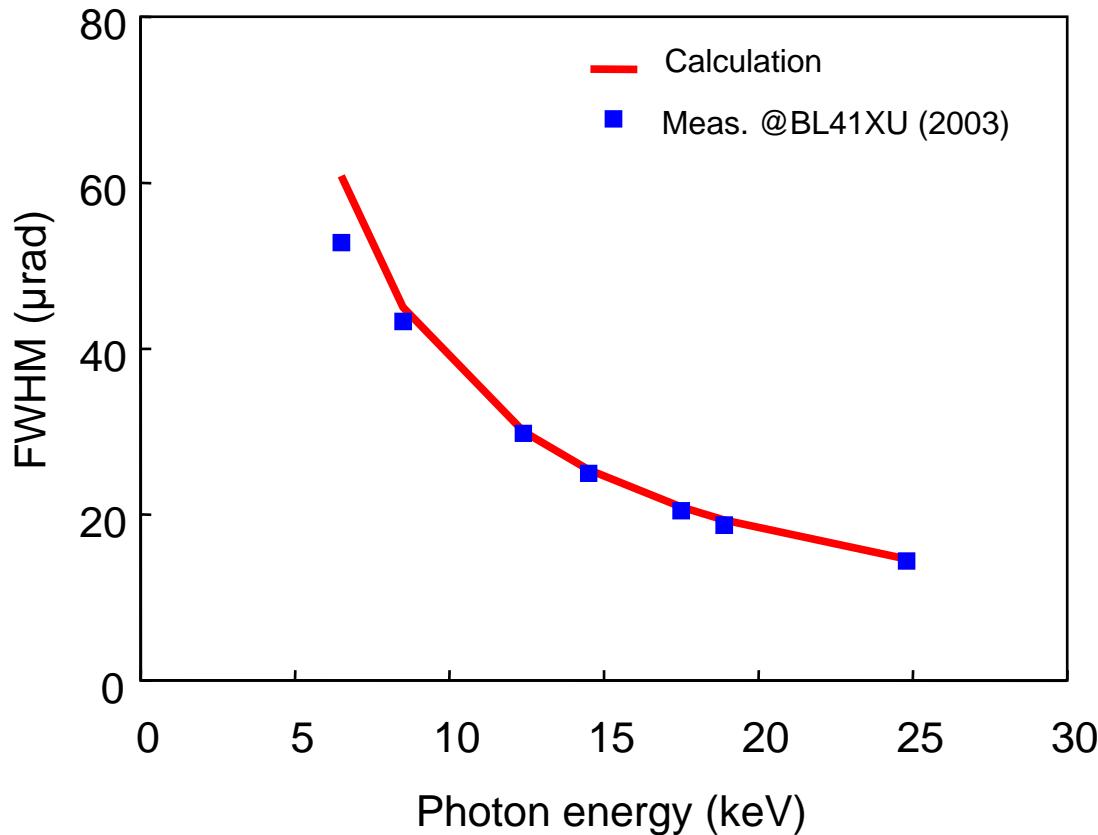
DCM view from upstream



Inside DCM: Stages + pin-post crystal

# Performance of pin-post crystal

---

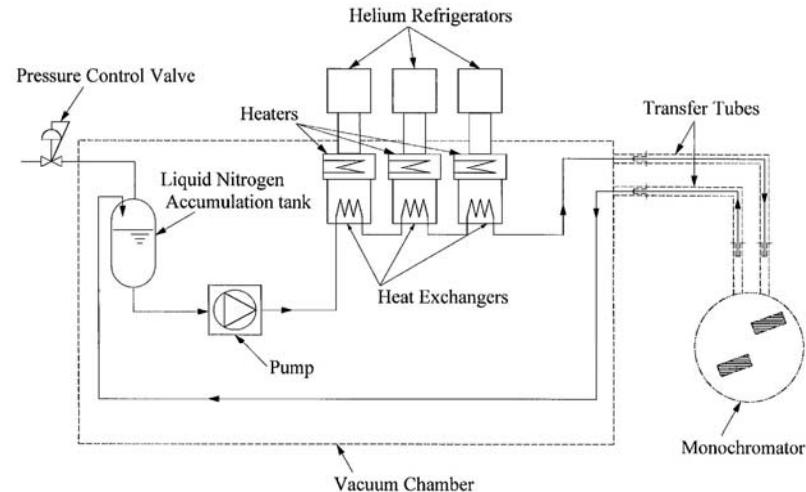
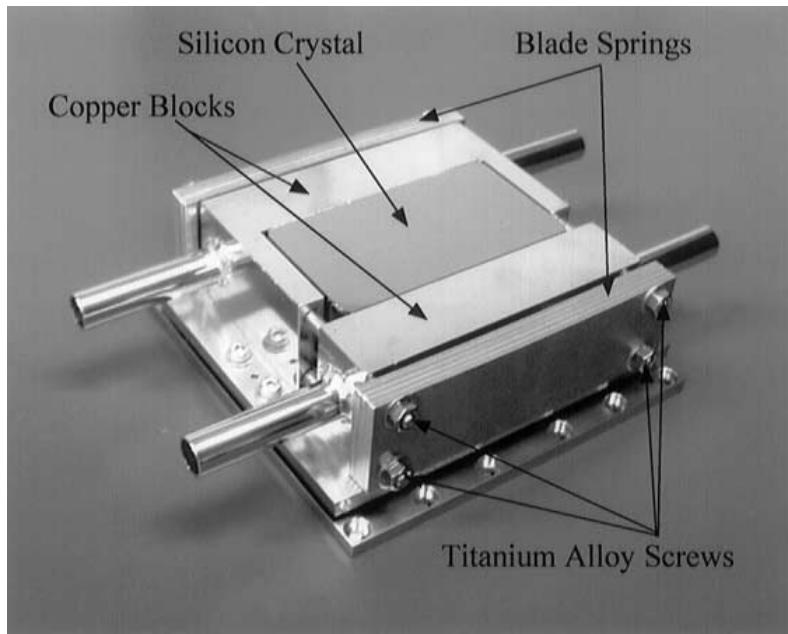


Rocking curve widths agree well.

# Cryogenic cooling

$\text{LN}_2$  circulator with He refrigerator

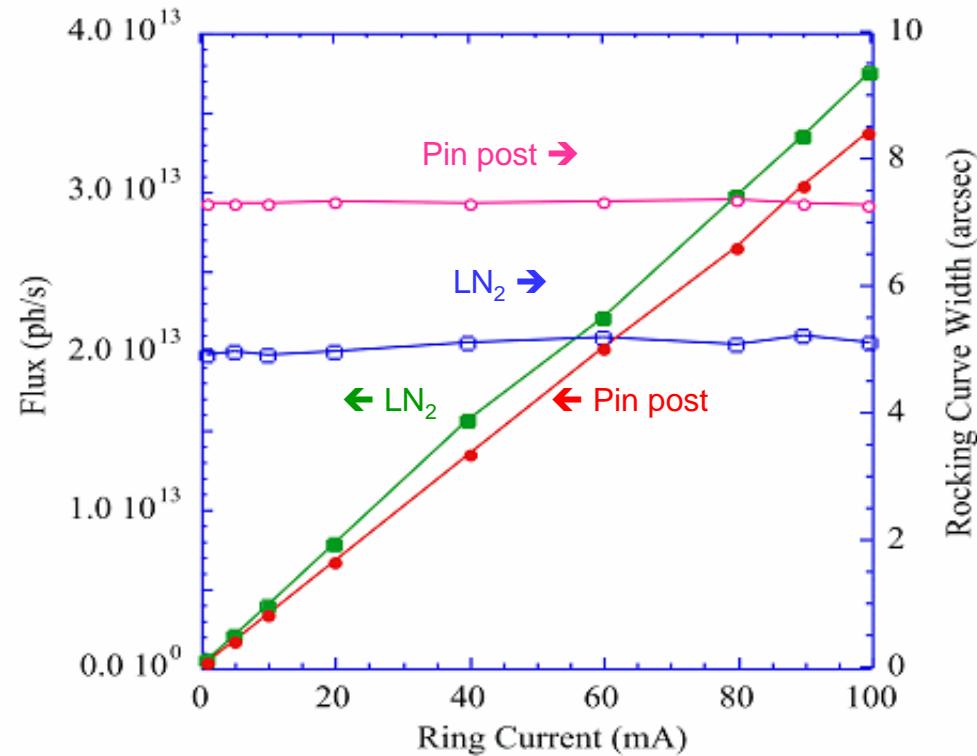
Indirect side cooling



Applied to undulator beamline

# Performance of pin-post cooling and cryogenic cooling

Heat load test (June 2000) up to 500 W, 500 W/mm<sup>2</sup>



# **Ila diamond indirect cooling**

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## **Merit:**

- Good thermal properties → Capability of indirect cooling
- Higher resolution ( $\leftrightarrow$  Less throughput (30~40% of Si))

## **Issues:**

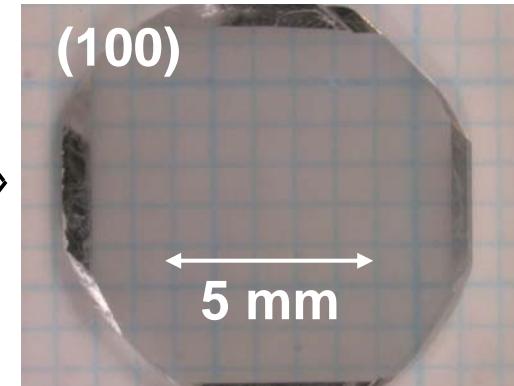
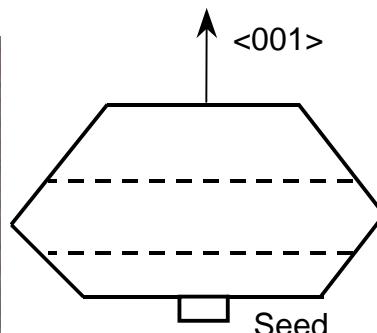
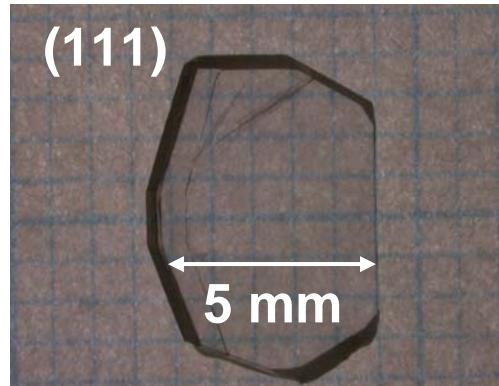
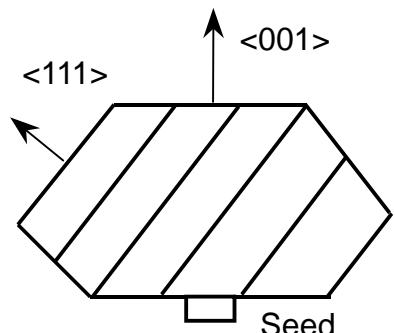
- Perfection of crystal → HPHT Ila diamond (Sumitomo)...  
Successive upgrade is crucial !
- Holding of crystal → X-ray topograph, Zygo
- Optimization of thermal contact → New process with In insert
- Small crystal (< 10 mm<sup>2</sup>)
- Alignment: using CCD camera, PIN photodiode, thermocouple

# Ila diamond crystal

Nearly perfect crystal using High Pressure High Temperature (HPHT) synthesis is available in <001> growth direction.

To maximize the photon flux, 111 refl. in Bragg case is used.

Effective size of Diamond (111) is, however, small !



Crystal handling is crucial:  
→ Mounting without strain  
→ Alignment

# Crystal mounting

## Thermal mounting method

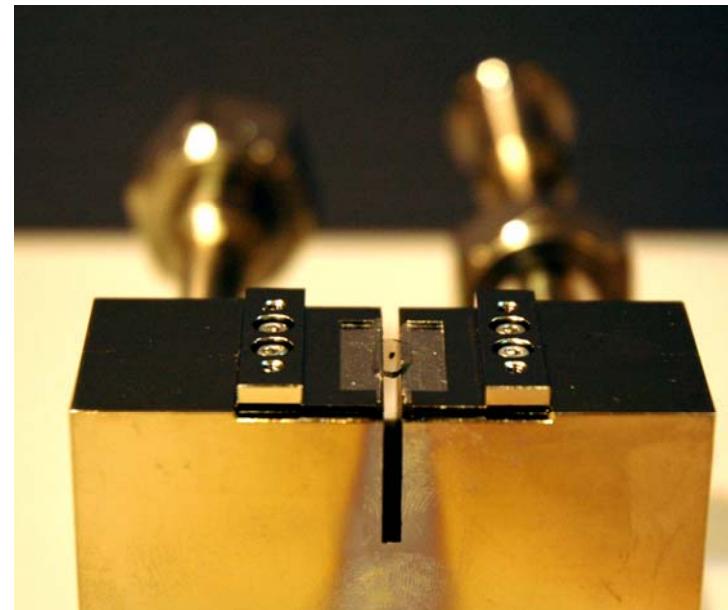
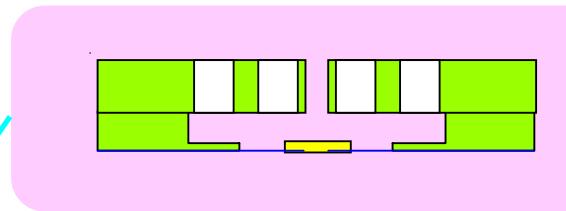
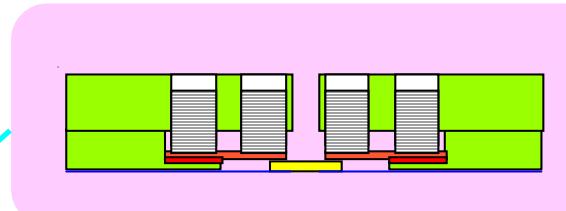
Mechanical mounting with  
SS plates and screws



Release the screws

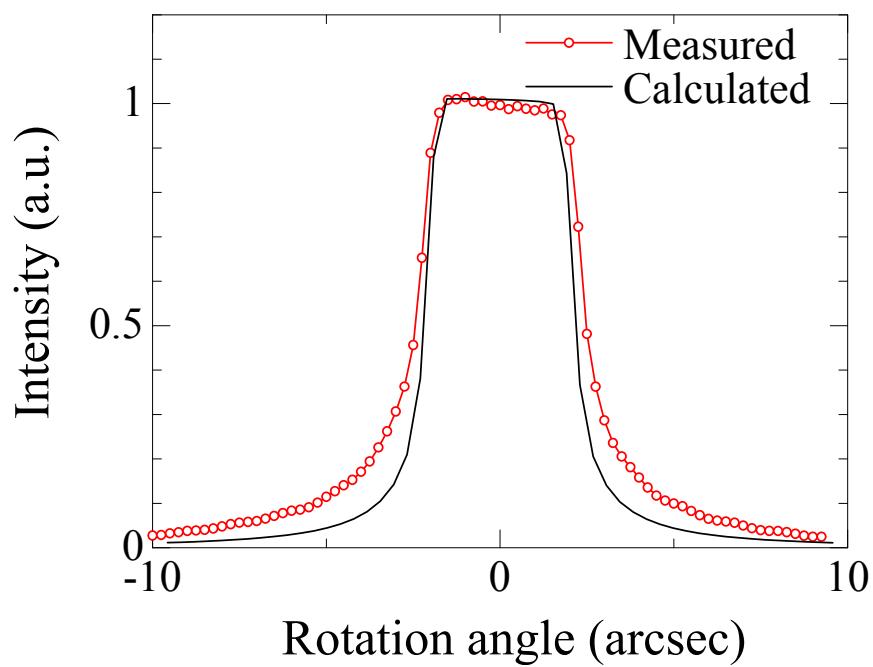
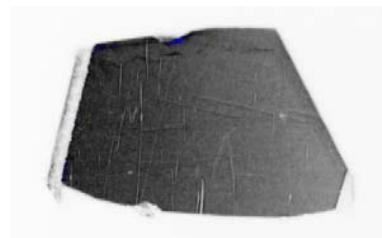


Temperature increase to ~ 130 °C  
Keep 30 min  
Decrease to room temperature



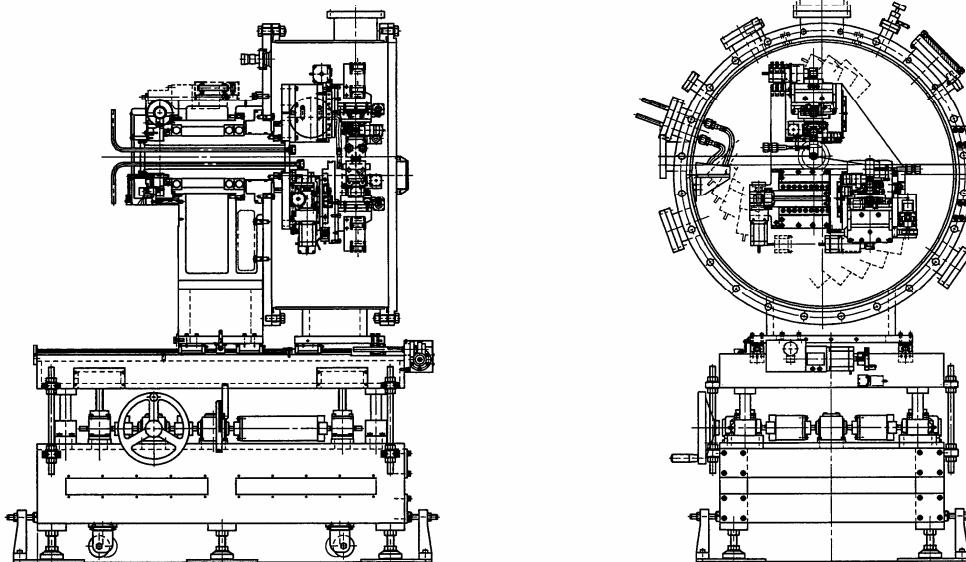
# Topograph and rocking curve

---



# Diamond monochromator (SPring-8 BL39XU)

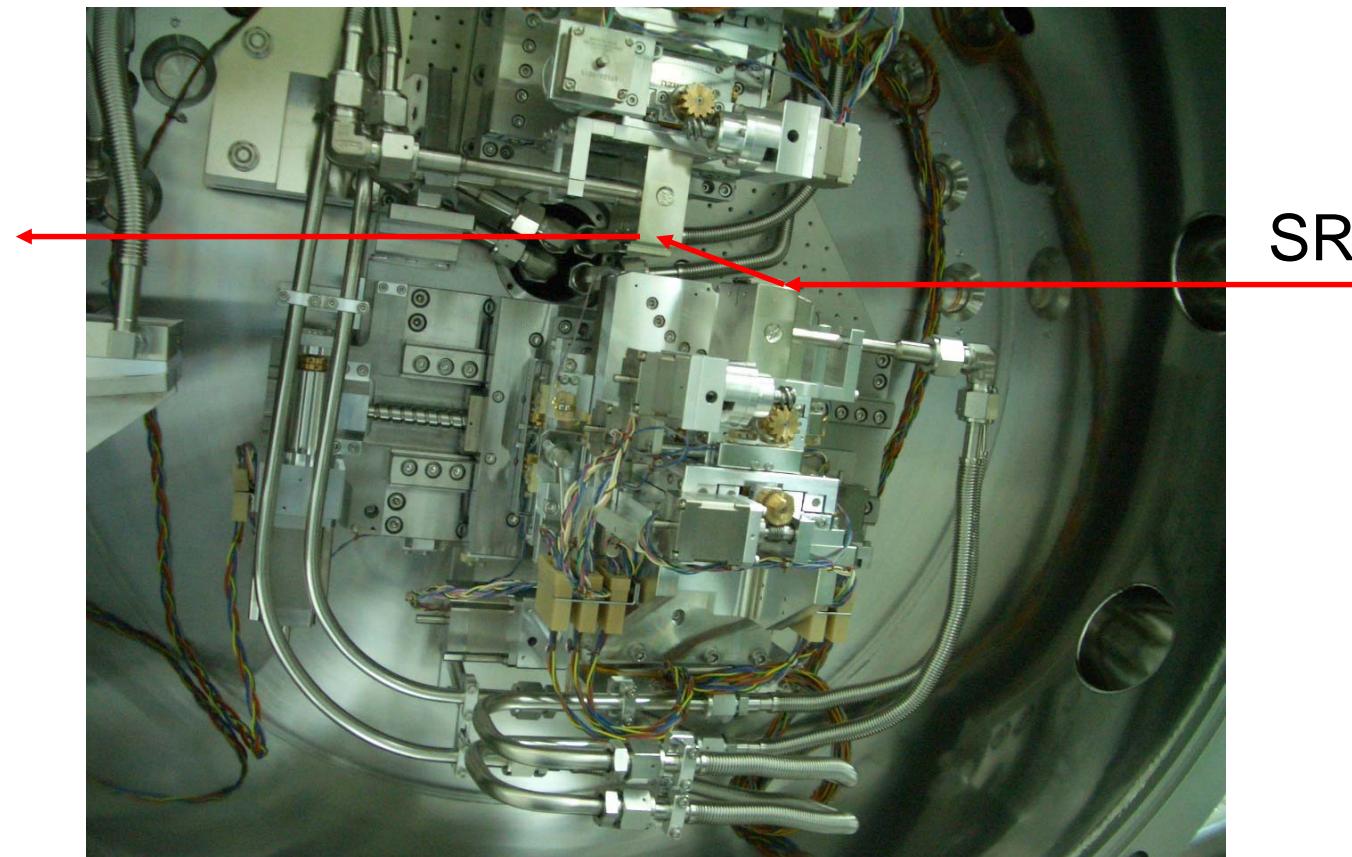
---



- Bragg angles:  $4.5 \sim 45^\circ$   
(Photon-energy compatible with silicon)
- $\theta$ -y-z computer link

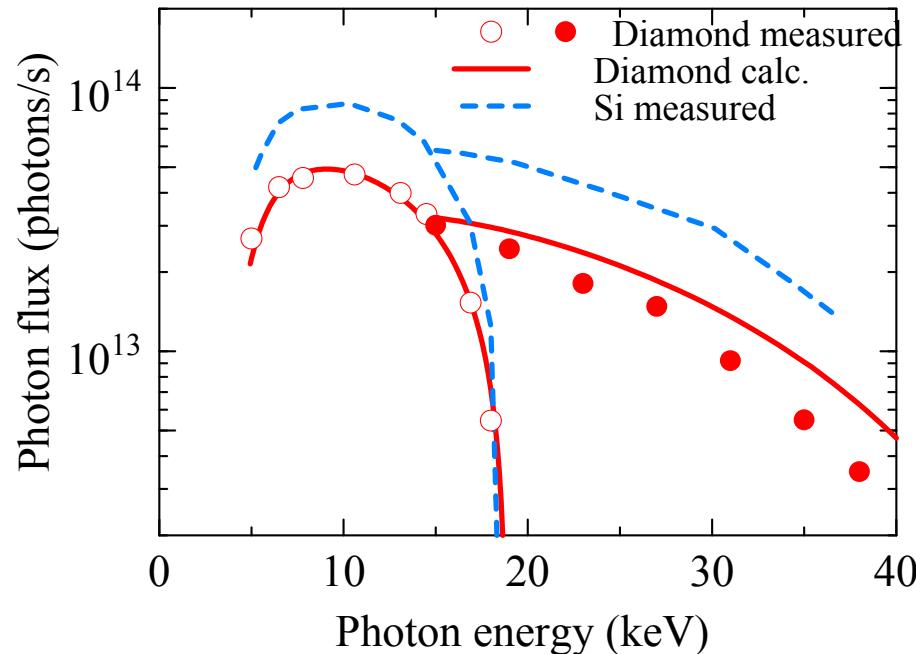
# Diamond monochromator (SPring-8 BL39XU)

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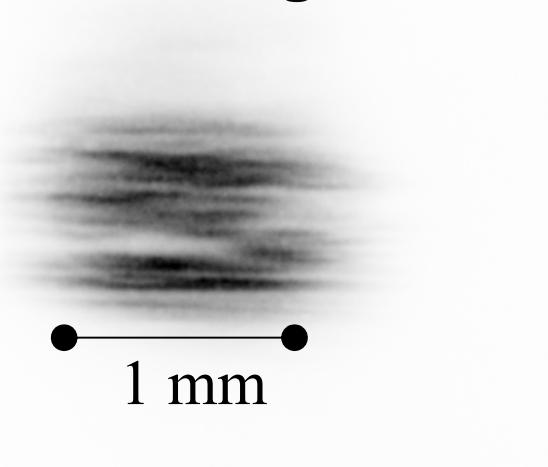


# Characterization of diamond monochromator

Photon flux



Beam image



$\varepsilon = 3$  nm. rad,  $I_b = 100$  mA

Front-end slit aperture = 0.7 (v) x 1.0 (h) mm<sup>2</sup>

Low energy: 50~60% of Si DCM

High energy: Infinite size effect ?

Improvement of crystal growth  
and surface finish is needed.

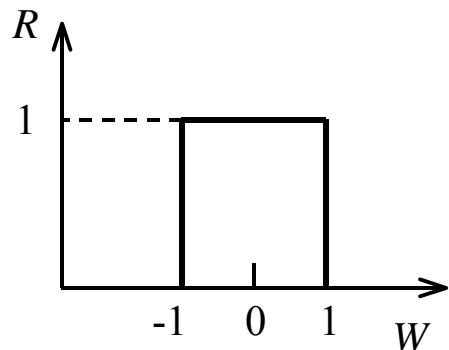
# **Efficiency with monochromator**

## **- Photon flux estimation -**

# Effective band width (Integrated intensity)

## Simple understanding

For top-hat shape, no absorption, sigma polarization, symmetric Bragg case



$$\left(\frac{\Delta E}{E}\right)_{\text{Eff}} = \frac{2|\chi_{hr}|}{\sin 2\theta_{\text{BK}}} \cot \theta_{\text{BK}}$$

$$= \frac{|\chi_{hr}|}{2 \sin^2 \theta_{\text{BK}}} \times 2$$

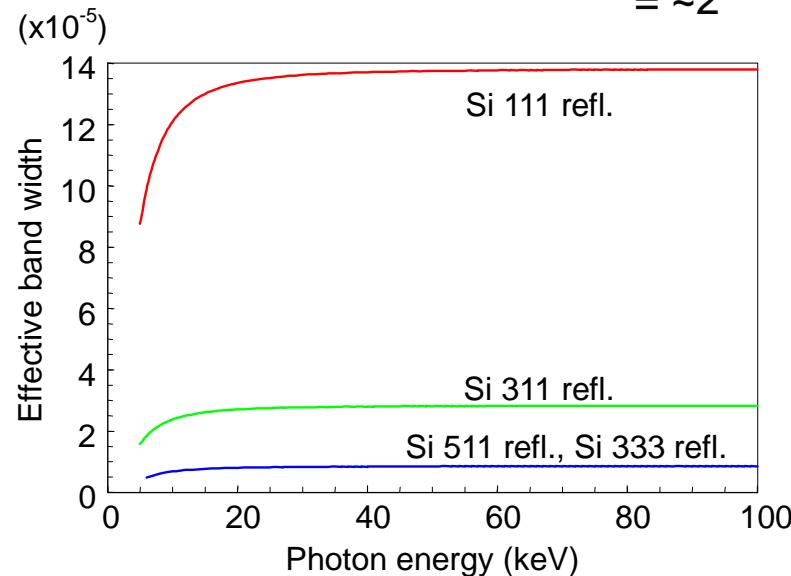
↑

= Energy resolution derived from Darwin width

## For double crystal monochromator

$$\left(\frac{\Delta E}{E}\right)_{\text{Eff}} = \frac{|\chi_{hr}|}{2 \sin^2 \theta_{\text{BK}}} \int R(W)^2 dW$$

$= \sim 2$



Effective band-width is obtained by integration of rocking curve.

When you need flux → Si 111 refl.

When you need resolution → Si 311, Si 511 refl.,..

# **Photon flux after monochromator**

---

Photon flux (throughput) after monochromator can be estimated by effective band width.

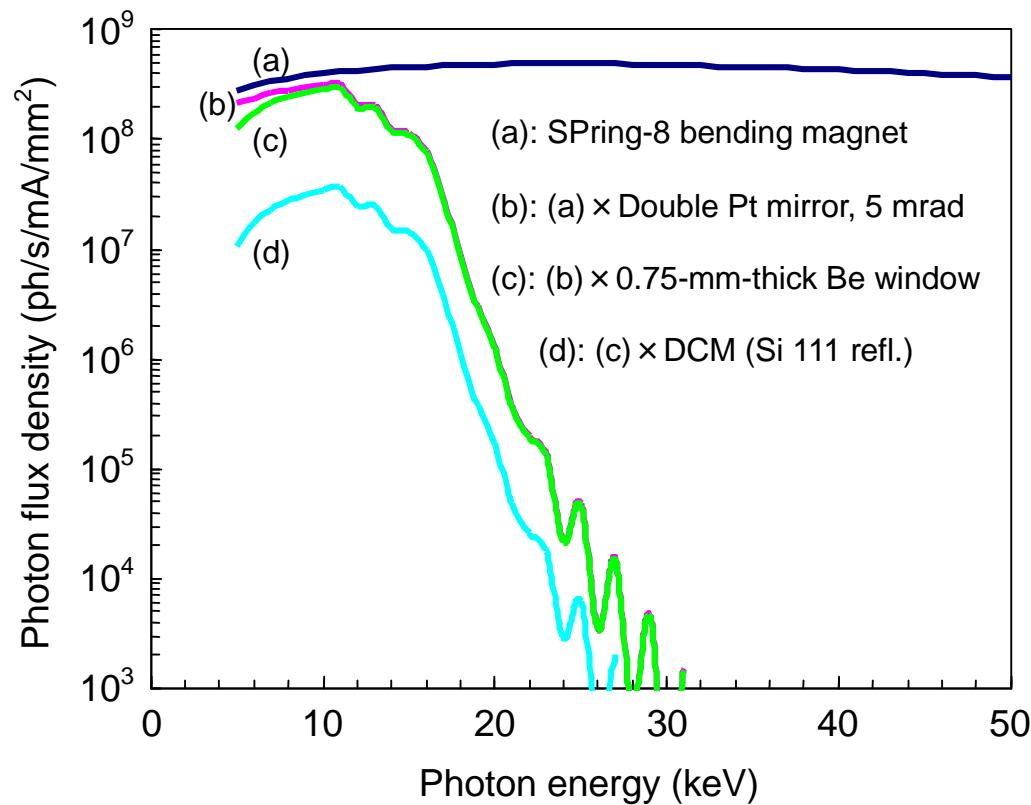
**Photon flux (ph/s) =**

**Photon flux from light source  
(ph/s/0.1%bw)**

**x 1000**

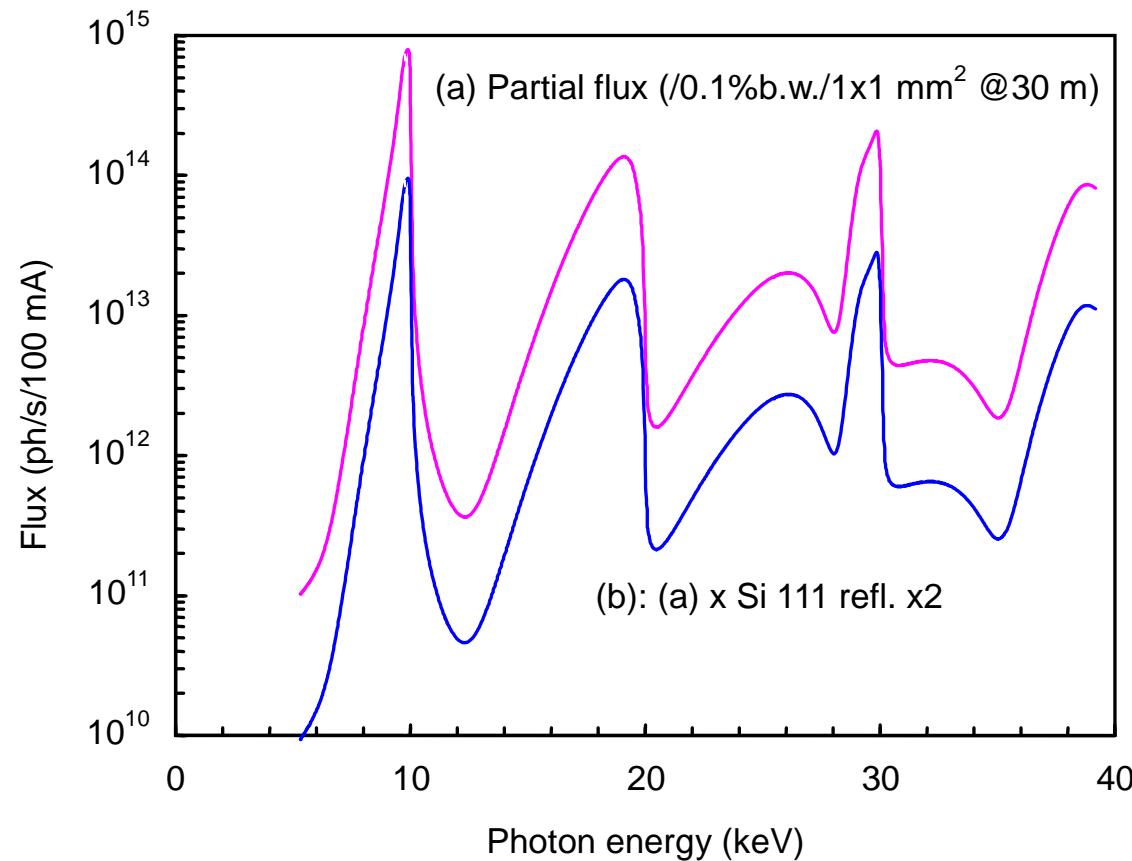
**x Effective band width of monochromator**

# Photon flux at bending magnet beamline



Example of photon flux estimation at bending magnet beamline BL02B1. (Photon flux density at 50 m from the source)

# Photon flux at undulator beamline



We can obtain photon flux of  $10^{13} \sim 10^{14}$  ph/s/100 mA/mm<sup>2</sup> using standard undulator sources and Si 111 reflections at SPring-8 beamlines.

# Other topics

# **Higher harmonics rejection**

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**For higher harmonics rejection**

**→ Total reflection mirror**

**→ Detuning of DCM**

# Total reflection mirror

---

## □ Substrate material

Si for white radiation

$\text{SiO}_2$  for monochromatic beam

## □ Coating material

Pt, Rh, Ni,...

Depending on energy, reflectivity, absorption edges,..

## □ Glancing angle

2~10 mrad (For SPring-8 X-ray beamline)

Depending on energy, reflectivity, absorption edges,..

## □ Mirror length

400 mm~1 m (For SPring-8 X-ray beamline)

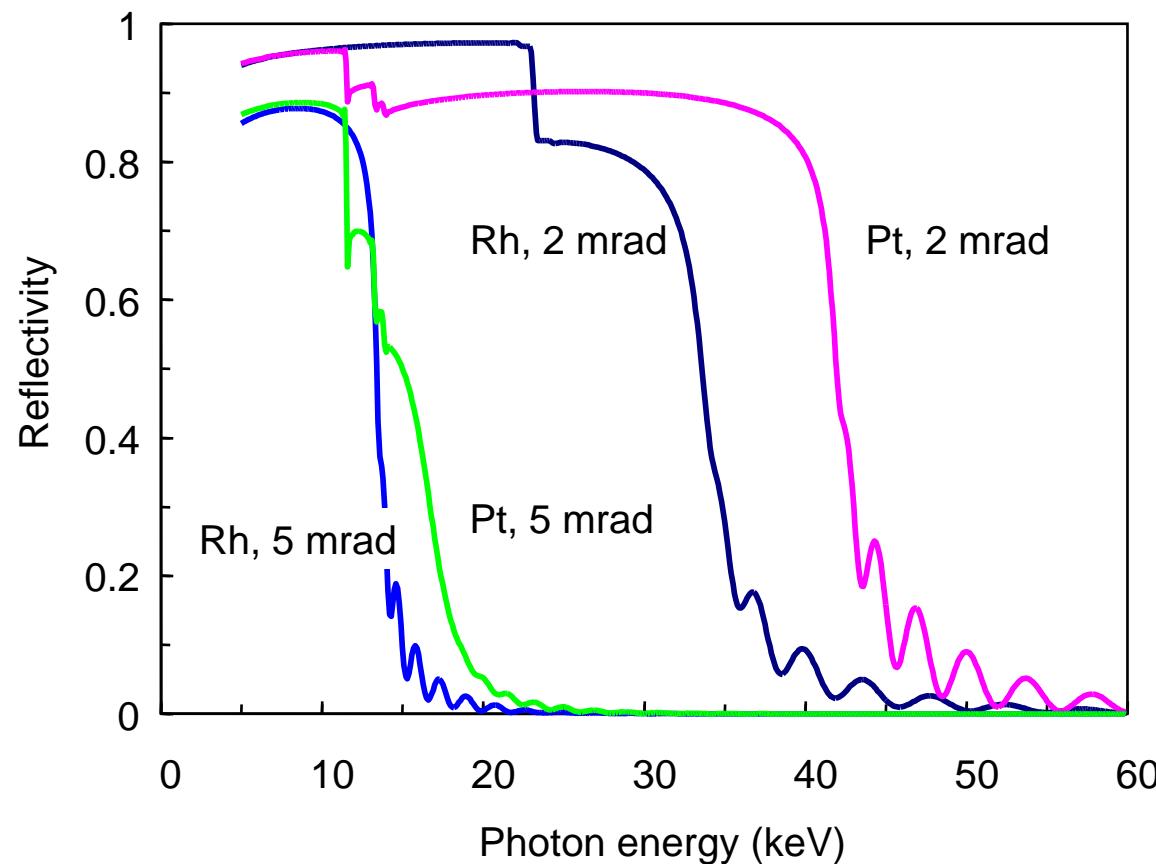
Depending on the beam size and glancing angle

e.g.  $100 \mu\text{rad} \times 50 \text{ m} / 5 \text{ mrad} = 1 \text{ m}$



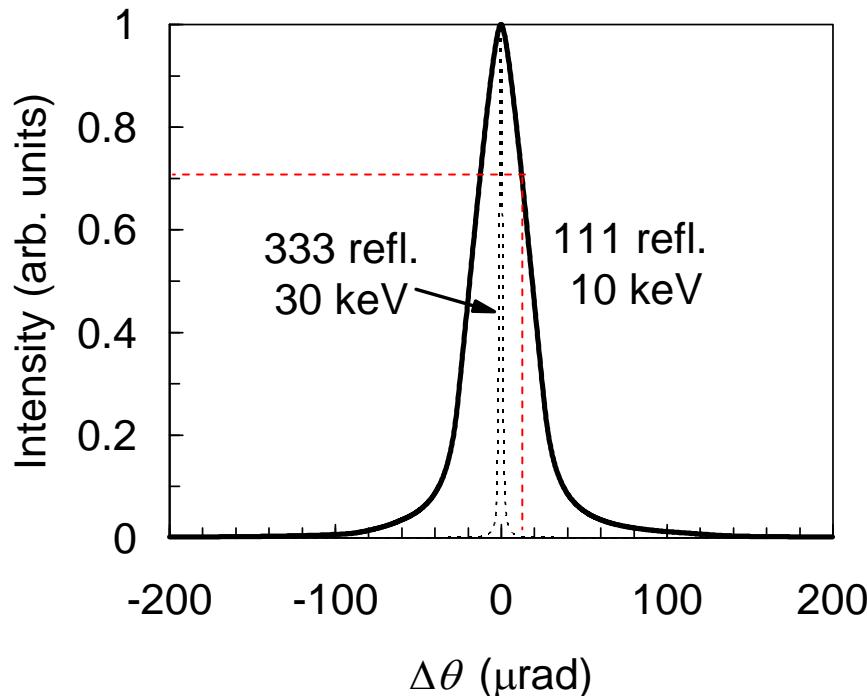
# Example of mirror reflectivity

---



Film thickness: 50 nm  
Surface roughness: 1 nm

# Detuning of DCM



e.g.  $\Delta\theta = 12 \mu\text{rad}$

→ 70% of peak intensity for fundamental (111 refl. @ 10 keV)

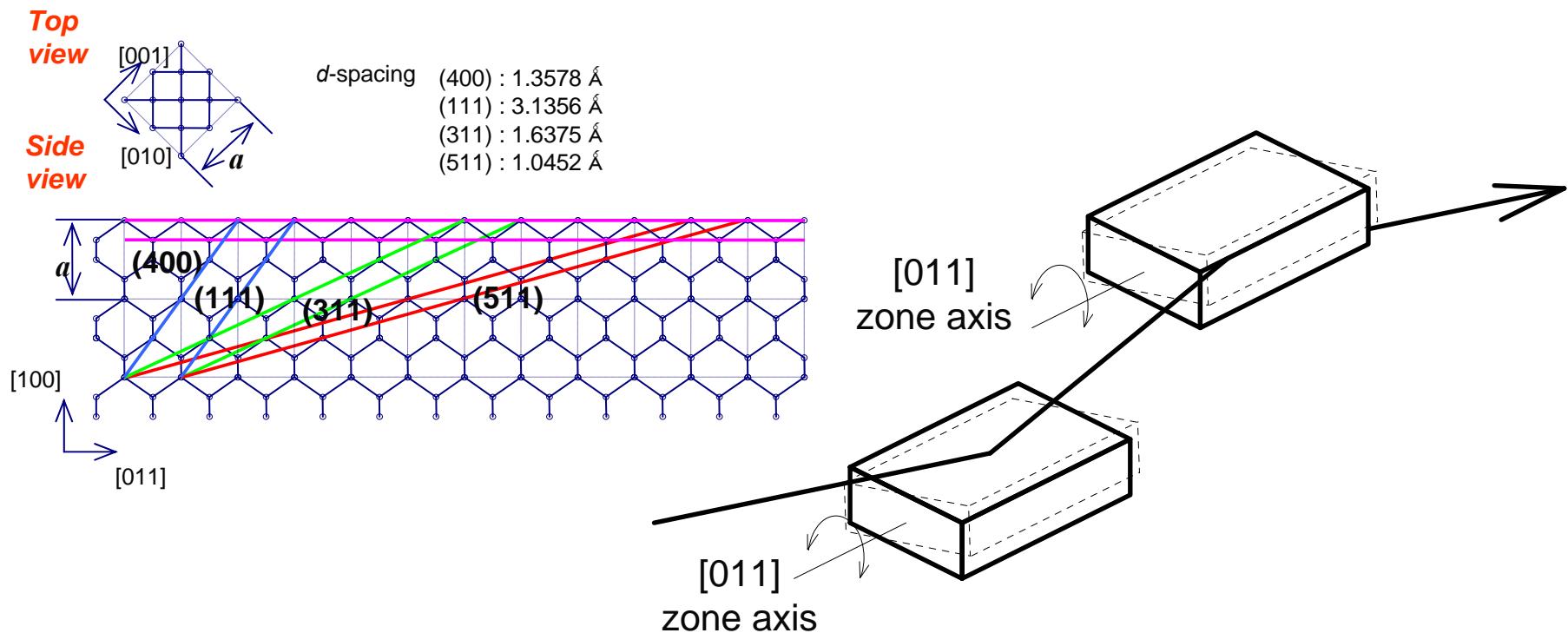
→ 0.3% of peak for 3rd harmonics (333 refl. @ 30 keV)

e.g.  $\Delta\theta_2 = 10 \mu\text{rad} \rightarrow$  Angle change of exit beam =  $2\Delta\theta_2 = 20 \mu\text{rad}$

Beam position change of 0.2 mm @ 10 m from DCM.

We should understand the beam position change by DCM detuning!

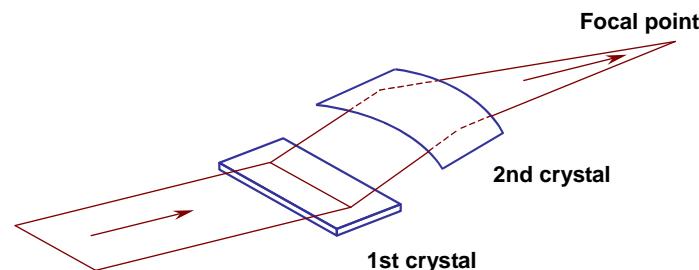
# Adjustable inclined geometry



We change the lattice plane by tilting the 1st and 2<sup>nd</sup> crystals simultaneously,  
and we can select 111 refl., 311 refl., 511 refl,...

# Sagittal focusing

## Principle of sagittal focusing



$$r = \frac{2pq}{p + q} \sin \theta$$

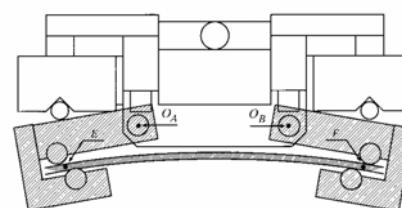
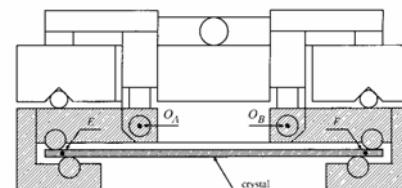
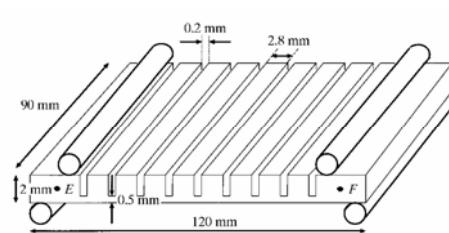
$r$ : radius of 2nd crystal

$\theta$ : Bragg angle

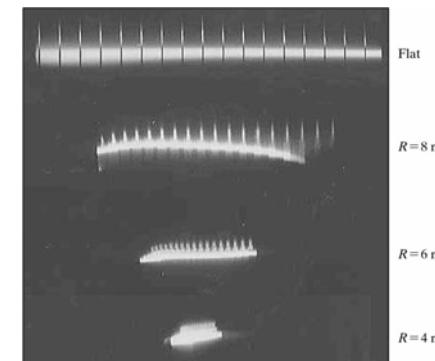
$p$ : source ~ crystal distance

$q$ : crystal ~ focal point distance

## Bending mechanism for SPring-8 sagittal focusing



## e.g. Sagittal focusing images



Si 311 refl.

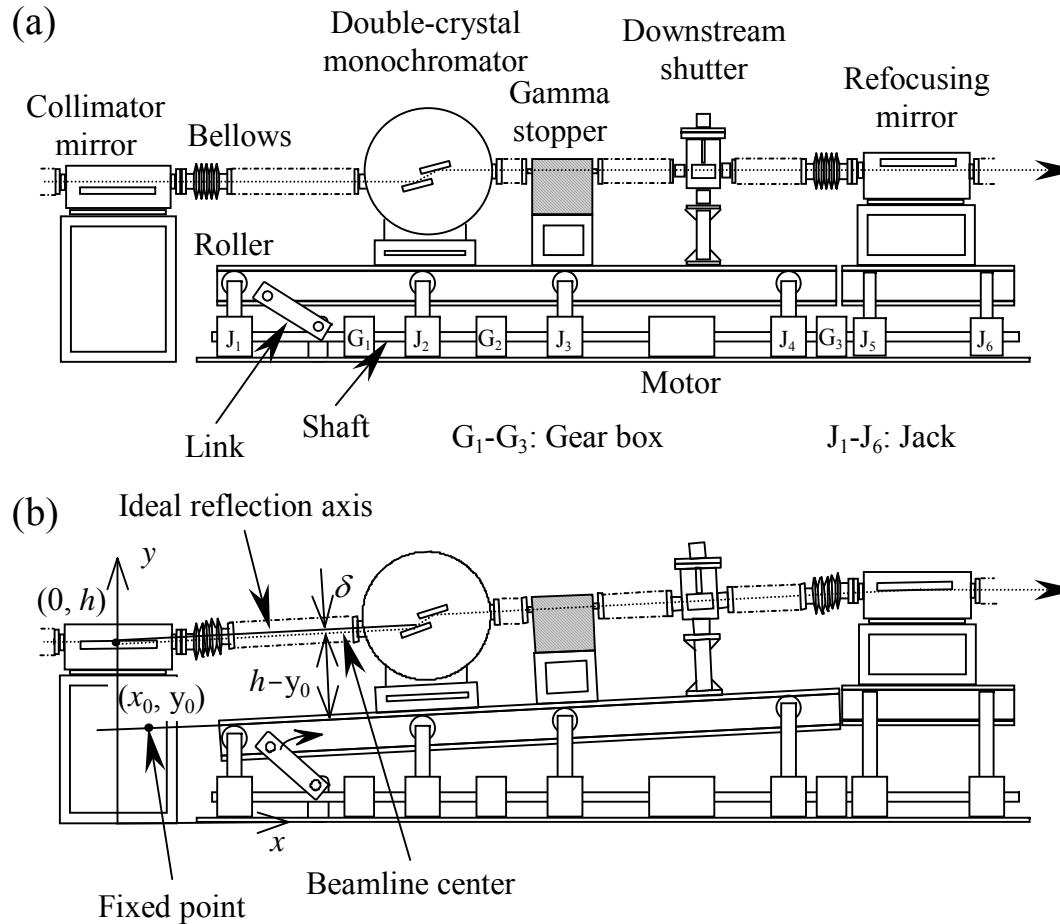
40 keV

Source ~ Crystal =  
36.5 m

Crystal ~ focal  
point = 16.5 m

Applied for bending magnet beamline

# Inclination stage and elevation stage for bending magnet beamlines



- For higher energy resolution using collimator mirror
- For higher photon flux using focusing mirrors
- For higher harmonics rejection

# Other issues (1)

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- Compton scattering shielding**

- Cooling for 2<sup>nd</sup> crystal, stages, and others

- Vibration control**

- Rigidity of stages → less number of stages
  - Coolant circulation, flexible tube,...

- Radiation damages**

- Degradation of rubber O-ring
  - Charge-up and damage to the control system

# Other issues (2)

---

- **Surface contamination**

- Vacuum quality → UHV monochromator
  - Recovering using ozone cleaning

- **Heat transfer analysis, simulation,  
fundamental data acquisition**

- Thermal conductivity measurement  
as material, surface roughness, pressure,  
temperature,...

# Issues in the future

---

- For more stable operation of monochromator
  - Vibration control (→ sub-microns, sub- $\mu$ rad)
  - Prevention of degradation due to radiation damage
- For better fabrication of crystal,
  - lower strain under high-heat-load condition
- For higher power and power density
- For wider energy range (→ lower, → higher)
- For higher energy resolution
- For 4GLS monochromator

*Thank you for your attention*